



Robotics 1

Robot components: Exteroceptive sensors

Prof. Alessandro De Luca

DIPARTIMENTO DI INGEGNERIA INFORMATICA
AUTOMATICA E GESTIONALE ANTONIO RUBERTI



SAPIENZA
UNIVERSITÀ DI ROMA



Summary

- force sensors
 - strain gauges and joint torque sensor
 - 6D force/torque (F/T) sensor at robot wrist
 - RCC = Remote Center of Compliance (*not a sensor, but similar...*)
- proximity/distance sensors ($\Rightarrow$ moved to AMR course!)
 - infrared (IF)
 - ultrasound (US)
 - laser
 - with structured light
- vision
- examples of robot sensor equipment
- some **videos** intertwined, with applications

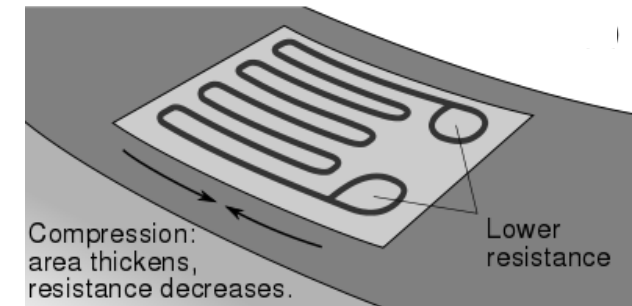
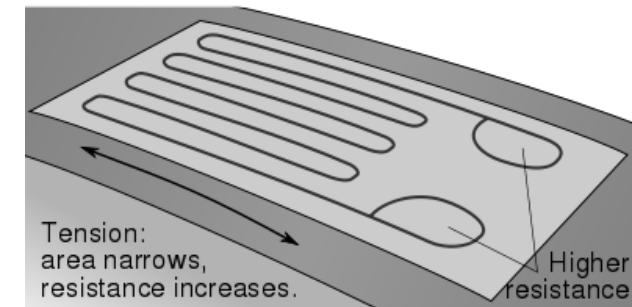
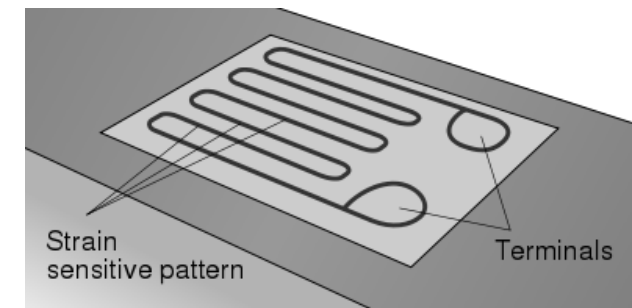
Force/torque and deformation

- indirect information obtained from the measure of **deformation** of an elastic element subject to the force or torque to be measured
- basic component is a **strain gauge**: it uses the variation of the resistance R of a metal conductor when its length L and/or cross-section S vary

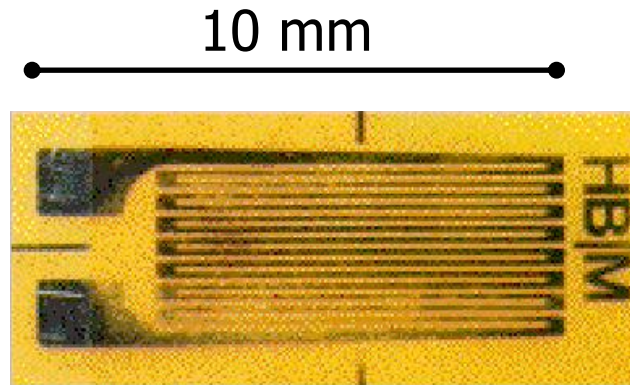
$$\frac{\partial R}{\partial L} > 0 \quad \frac{\partial R}{\partial S} < 0$$

$$\frac{\partial R}{\partial T} \text{ small}$$

temperature



Strain gauges



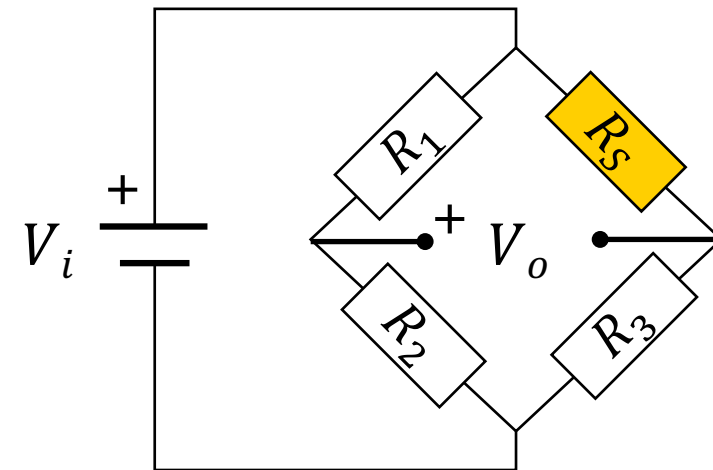
principal measurement axis

$$\text{Gauge-Factor} = GF = \frac{\Delta R/R}{\Delta L/L} \leftarrow \text{strain } \varepsilon$$

(typically $GF \approx 2$, i.e., small sensitivity)

if R_1 has the same dependence on T of R_S
thermal variations are automatically compensated

Wheatstone **single-point** bridge connection
(for accurately measuring resistance)



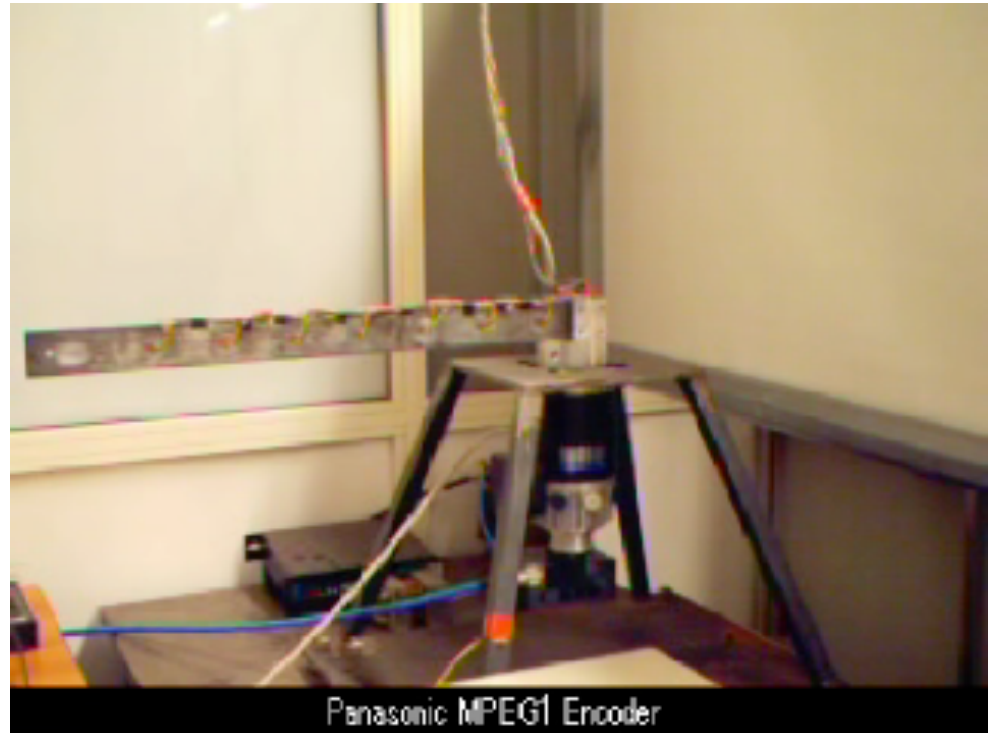
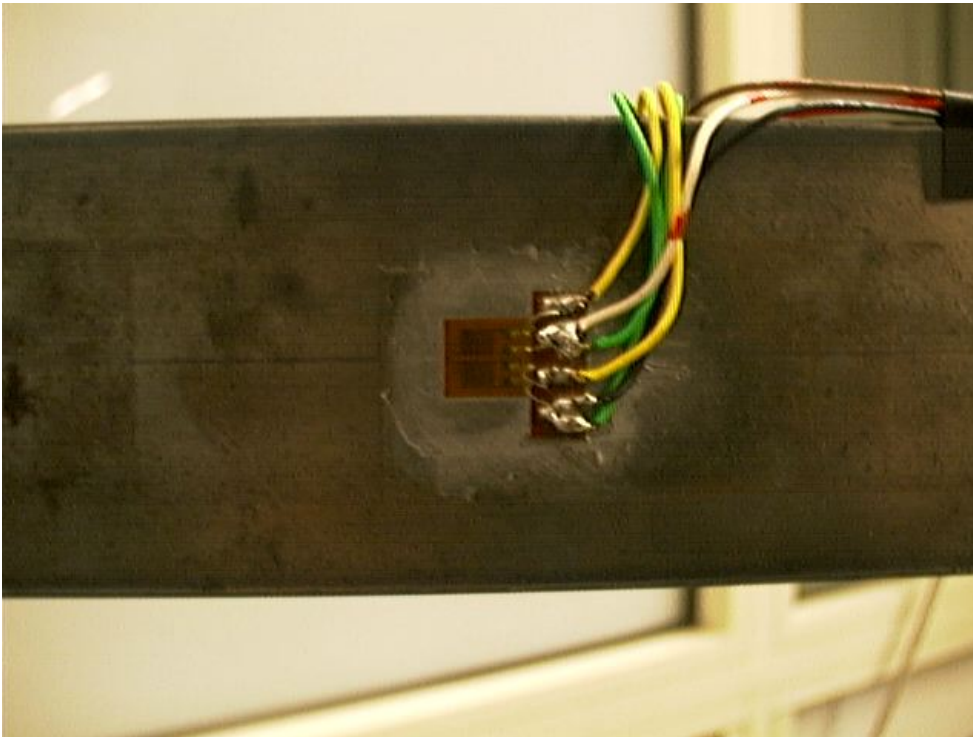
- R_1, R_2, R_3 very well matched ($\approx R$)
- $R_S \approx R$ at rest (no stress)
- **two-point** bridges have 2 strain gauges connected oppositely (↗ sensitivity)

$$V_0 = \left(\frac{R_2}{R_1 + R_2} - \frac{R_3}{R_3 + R_S} \right) V_i$$



Strain gauges in flexible arms

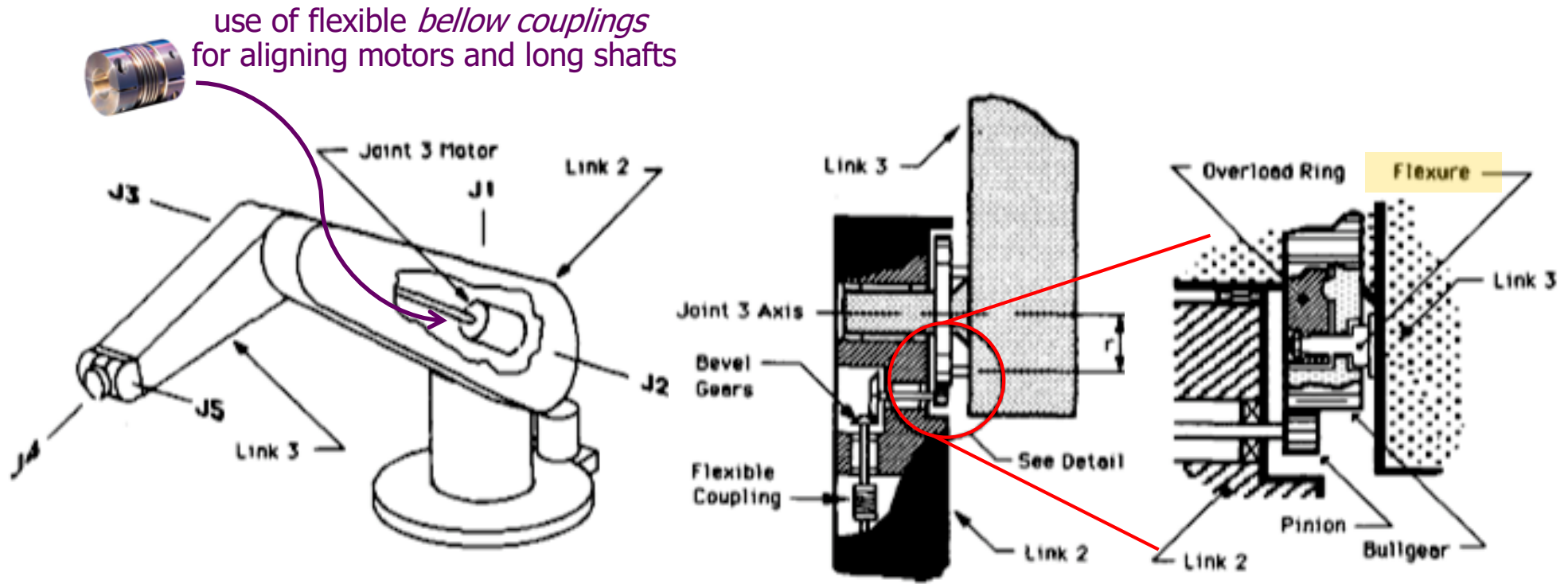
video



7 strain gauges glued⁽¹⁾ to a flexible aluminum beam (a robot “link”) measuring its local “curvature” in dynamic bending during slew motions (a **proprioceptive** use of these sensors)

⁽¹⁾ by cyanoacrylic glue

Torque sensor at robot joints



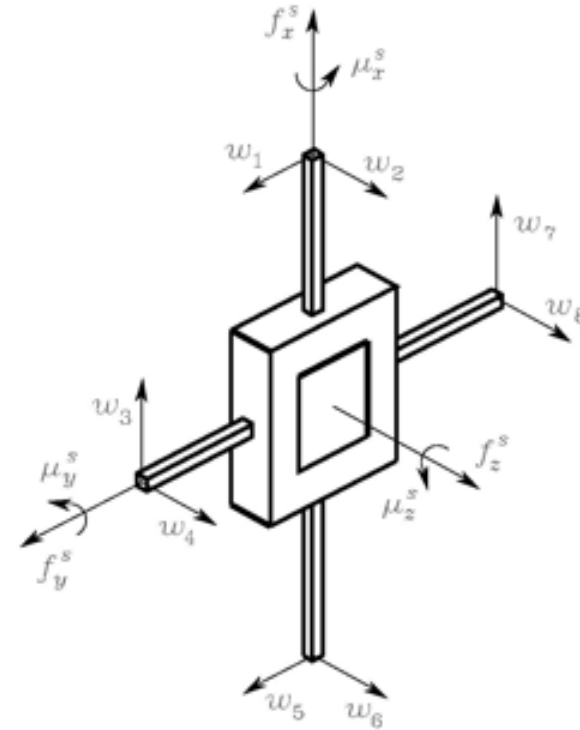
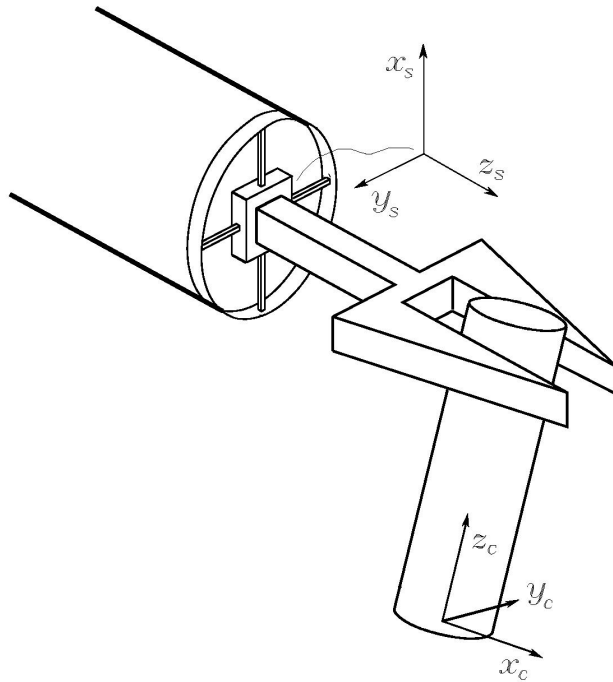
strain gauge mounted to “sense” the axial deformation of the transmission shaft of joint #3 (elbow) in a PUMA 500 robot (again, a **proprioceptive** use of this sensor)



Force/torque sensor at robot wrist

- a device (with the outer form of a cylinder), typically located between the last robot link and its end-effector
- top and bottom plates are mechanically connected by a number of **deformable elements** subject to **strain** under the action of forces and moments
- there should be at least one such element in any direction along/around which a force or torque measure is needed
- since a complete “decoupling” of these measurements is hard to obtain, there are $N \geq 6$ such deformable elements
- on each element, a **pair of strain gauges** is glued so as to undergo opposite deformations (e.g., traction/compression) along the main axis of measurement

Maltese-cross configuration



- diameter ≈ 10 cm
- height ≈ 5 cm
- $50 \div 500$ N (resolution 0.1%)
- $5 \div 70$ Nm (resolution 0.05%)
- sample frequency ≈ 1 KHz

- 4 deformable elements
- two pairs of strain gauges are mounted on opposite sides of each element (8 pairs)
- the two gauges of each pair are placed adjacent on the same Wheatstone bridge

6D force/torque sensors

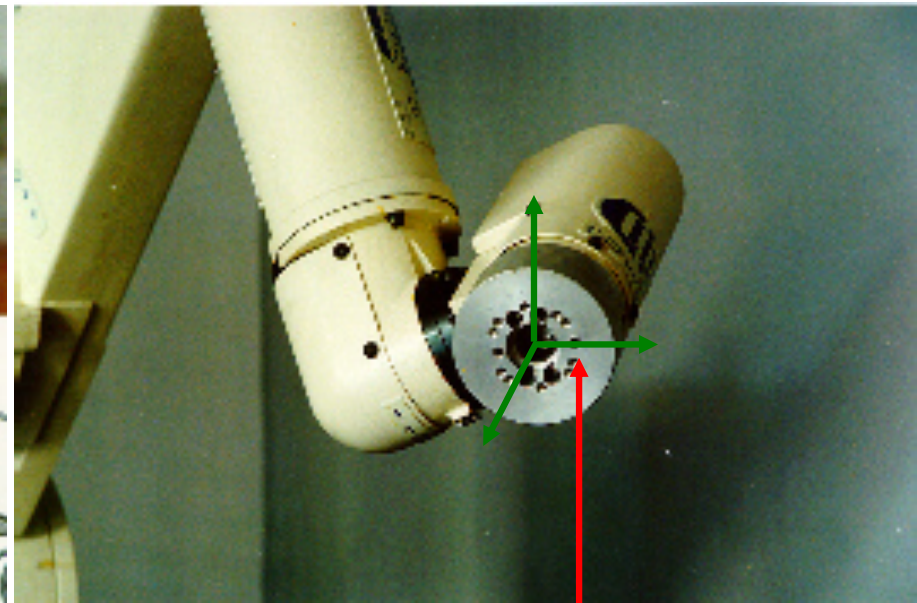
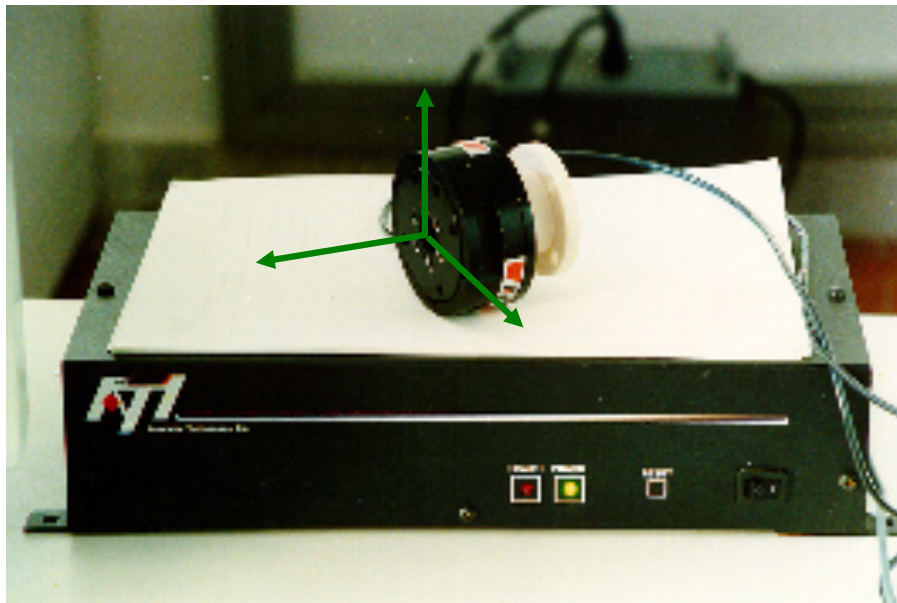
- ATI series
- cost (in 2016): about 6 K€ for Mini45 model + 700 € DAQ card



Model	Max Fx,Fy*	Max Tx,Ty*	Weight**	Diameter**	Height**
Nano17	±50 N	±500 N-mm	0.0091 kg	17 mm	14 mm
Nano25	±250 N	±6 N-m	0.064 kg	25 mm	22 mm
Nano43	±36 N	±500 N-mm	0.041 kg	43 mm	11 mm
Mini40	±80 N	±4 N-m	0.05 kg	40 mm	12 mm
Mini45	±580 N	±20 N-m	0.091 kg	45 mm	16 mm
Gamma	±130 N	±10 N-m	0.25 kg	75 mm	33 mm
Delta	±660 N	±60 N-m	0.91 kg	94 mm	33 mm
Theta	±2500 N	±400 N-m	5 kg	150 mm	61 mm
Omega160	±2500 N	±400 N-m	2.7 kg	160 mm	56 mm
Omega190	±7200 N	±1400 N-m	6.4 kg	190 mm	56 mm

6D force/torque sensor

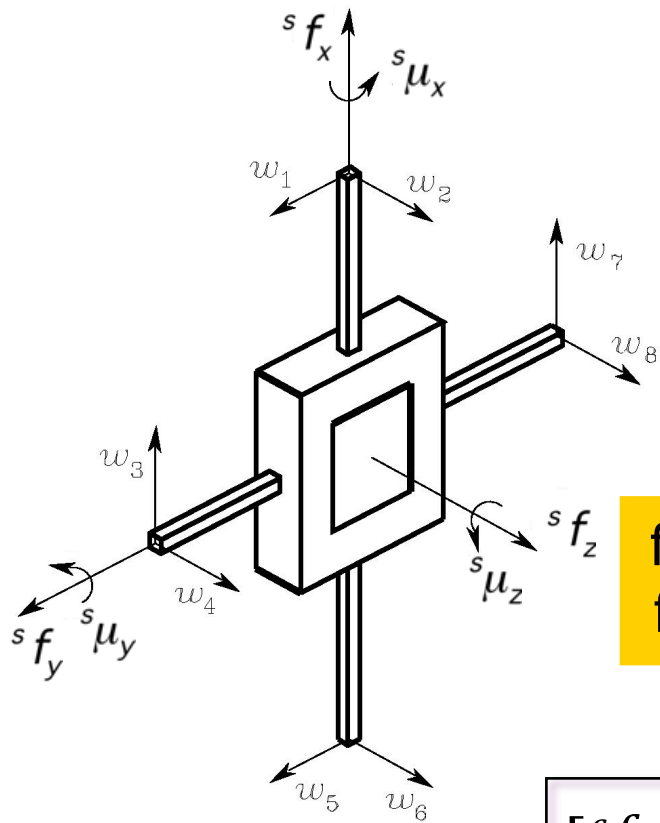
- electronic processing unit and mounting on an industrial robot (Comau Smart 3 robot, 6R kinematics)



mounting flange
(on link 6 of the manipulator arm)



6D F/T sensor calibration



$$\begin{bmatrix} s f_x \\ s f_y \\ s f_z \\ s \mu_x \\ s \mu_y \\ s \mu_z \end{bmatrix} = \begin{bmatrix} 0 & 0 & c_{13} & 0 & 0 & 0 & c_{17} & 0 \\ c_{21} & 0 & 0 & 0 & c_{25} & 0 & 0 & 0 \\ 0 & c_{32} & 0 & c_{34} & 0 & c_{36} & 0 & c_{38} \\ 0 & 0 & 0 & c_{44} & 0 & 0 & 0 & c_{48} \\ 0 & c_{52} & 0 & 0 & 0 & c_{56} & 0 & 0 \\ c_{61} & 0 & c_{63} & 0 & c_{65} & 0 & c_{67} & 0 \end{bmatrix} \begin{bmatrix} w_1 \\ w_2 \\ w_3 \\ w_4 \\ w_5 \\ w_6 \\ w_7 \\ w_8 \end{bmatrix}$$

force/torque measured in the frame attached to the sensor

calibration matrix

output of Wheatstone bridges

$$\begin{bmatrix} {}^c f_c \\ {}^c \mu_c \end{bmatrix} = \begin{bmatrix} {}^c R_s & O \\ S({}^c r_{cs}) {}^c R_s & {}^c R_s \end{bmatrix} \begin{bmatrix} s f_s \\ s \mu_s \end{bmatrix}$$

transformation from the sensor frame to the load/contact frame (at TCP)

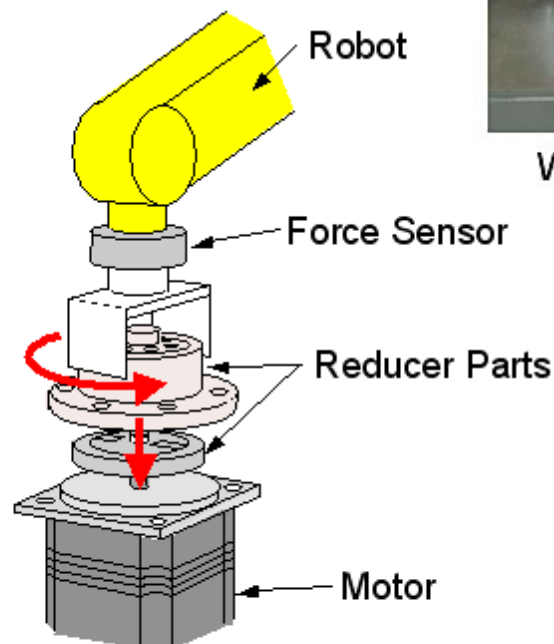
Typical uses of a F/T sensor



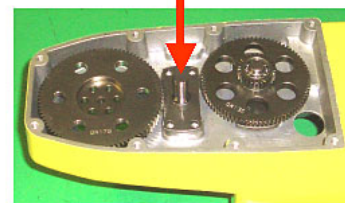
Washstand



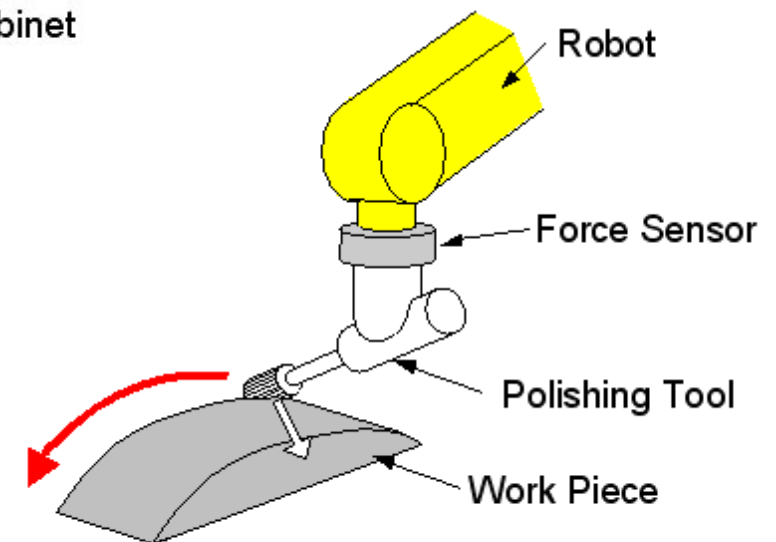
Metal Cabinet



Phase matching by force sensing



Gear Parts



Following with constant pushing force

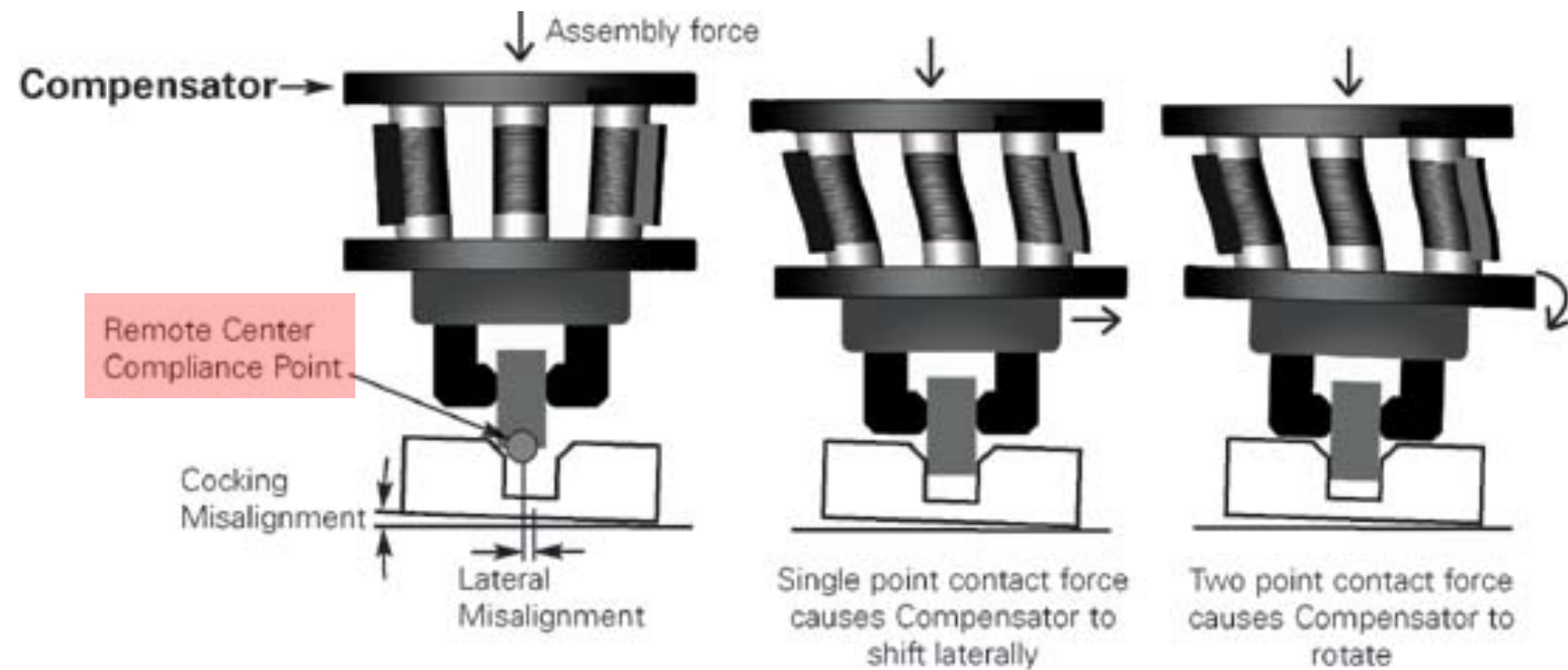


Passive RCC device

- RCC = Remote Center of Compliance
- placed on the wrist so as to introduce **passive "compliance"** to the robot end-effector, in response to static forces and moments applied from the environment at the contact area
- mechanical construction yields **"decoupled"** linear/angular motion responses **if** contact occurs at or near the RCC point

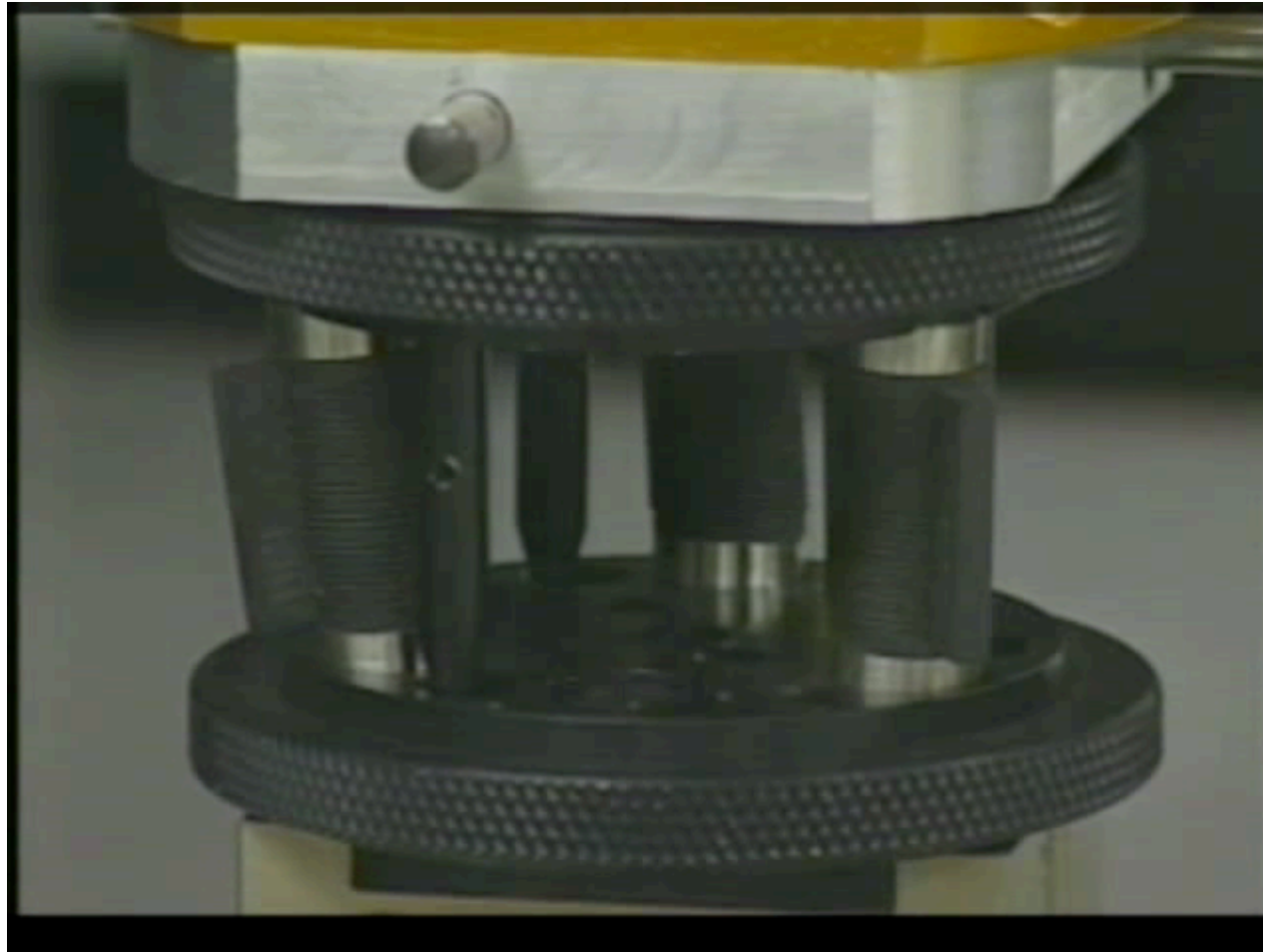


Assembly with RCC





Passive assembly with RCC



video

RCC by ATI Industrial Automation
<http://www.ati-ia.com>



Active assembly with F/T sensor

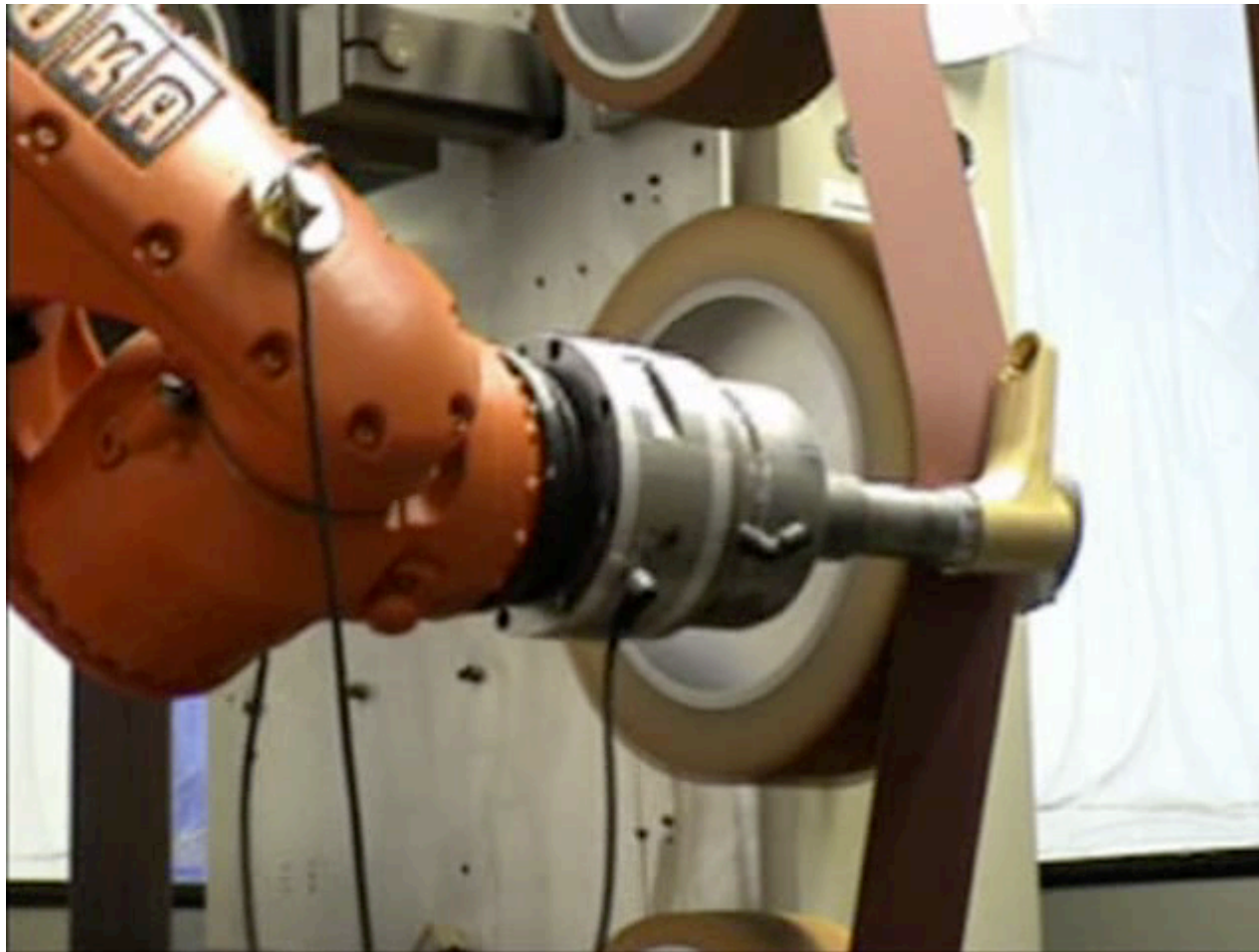


video

ABB robot with ATI F/T sensor



Surface finishing with F/T sensor

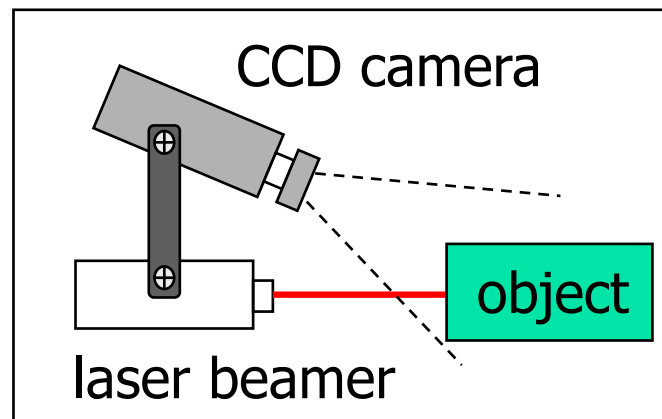


video

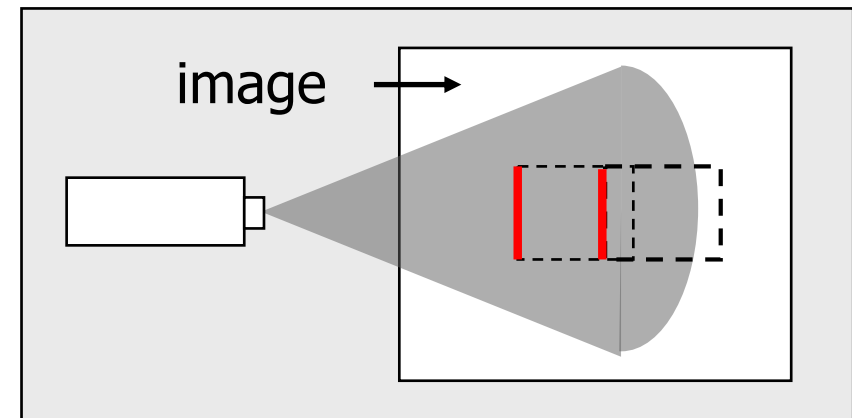
KUKA robot with F/T sensor

Proximity/distance sensors - 4

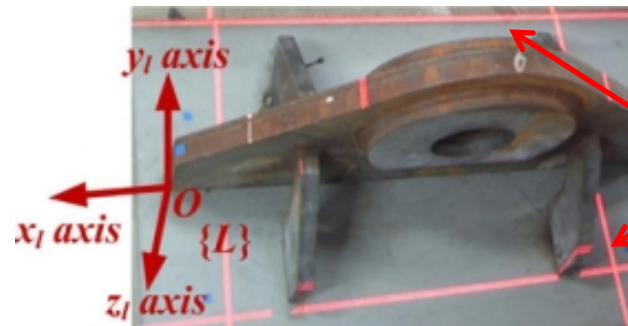
- **structured light:** a laser beam (coherent light source) is projected on the environment, and its planar intersection with surrounding objects is detected by a (tilted) camera
- the position of the “red pixels” on the camera image plane is in **trigonometric** relation with the object distance from the sensor



side view

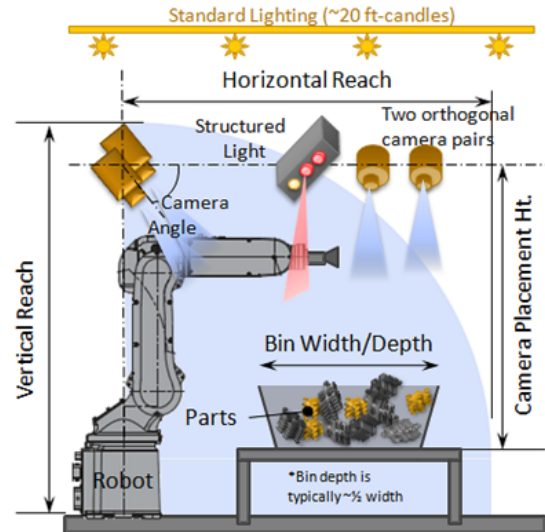


top view



projected laser beams
(2D in this case)

Use of structured light sensors



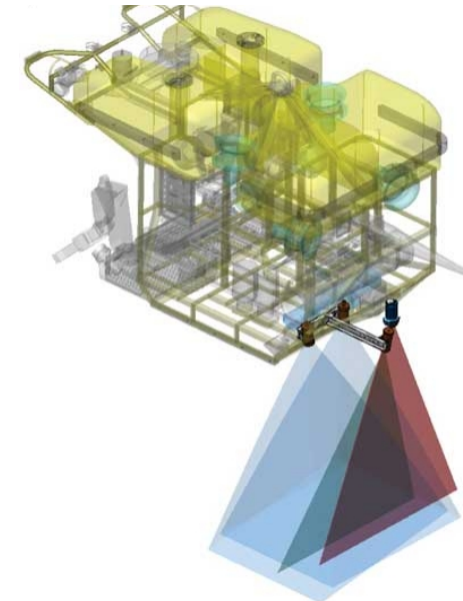
Random **bin picking** of 10-30 parts/minute (with surface inspection) with a 6R industrial robot, two pairs of cameras and a structured light sensor [Universal Robotics]



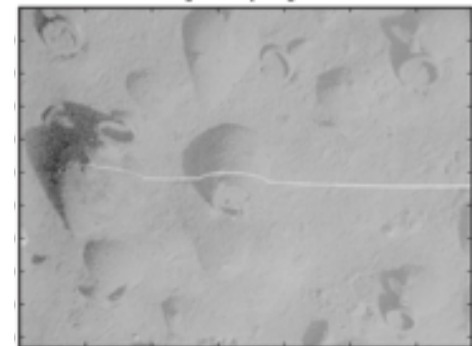
Structured light approach to best fit and **finish car bodies** (down to 0.1 mm) for reducing wind noise [Ford Motor Co.]



Virtobot system for post-mortem 3D optical scanning of human body & image-guided needle placement [Univ. Zürich]



Hercules ROV + structured-laser-light imaging system for high-resolution bathymetric underwater maps [Univ. Rhode Island]



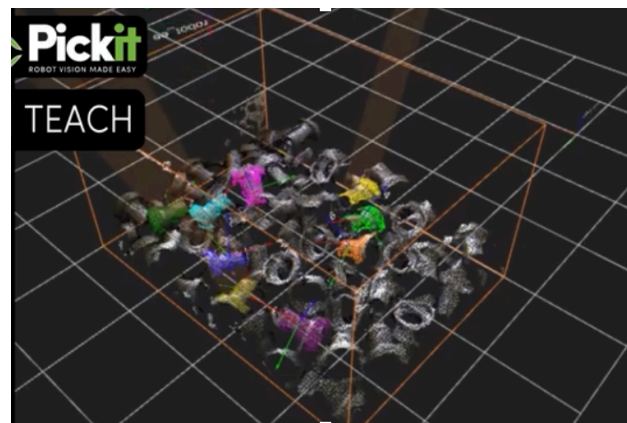
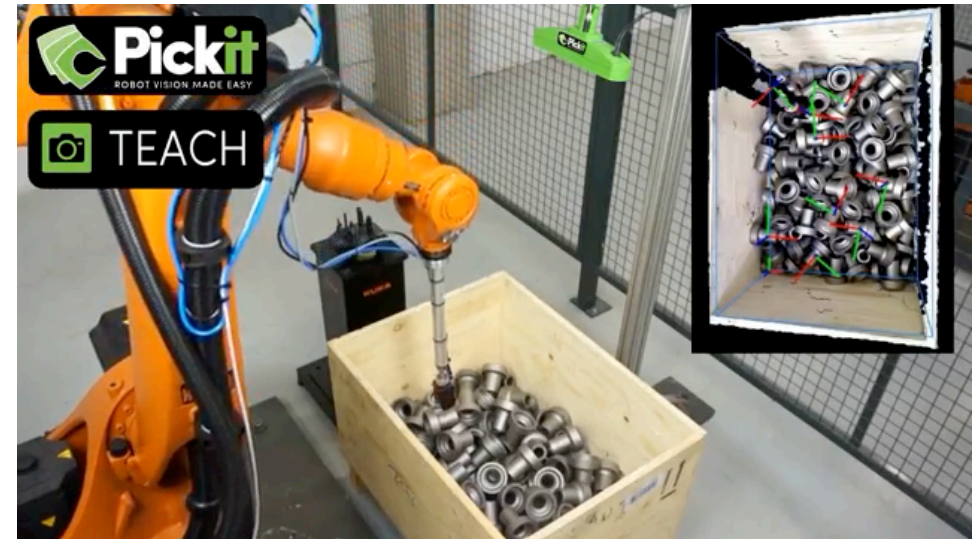
Robotic bin picking using vision and structured light



video

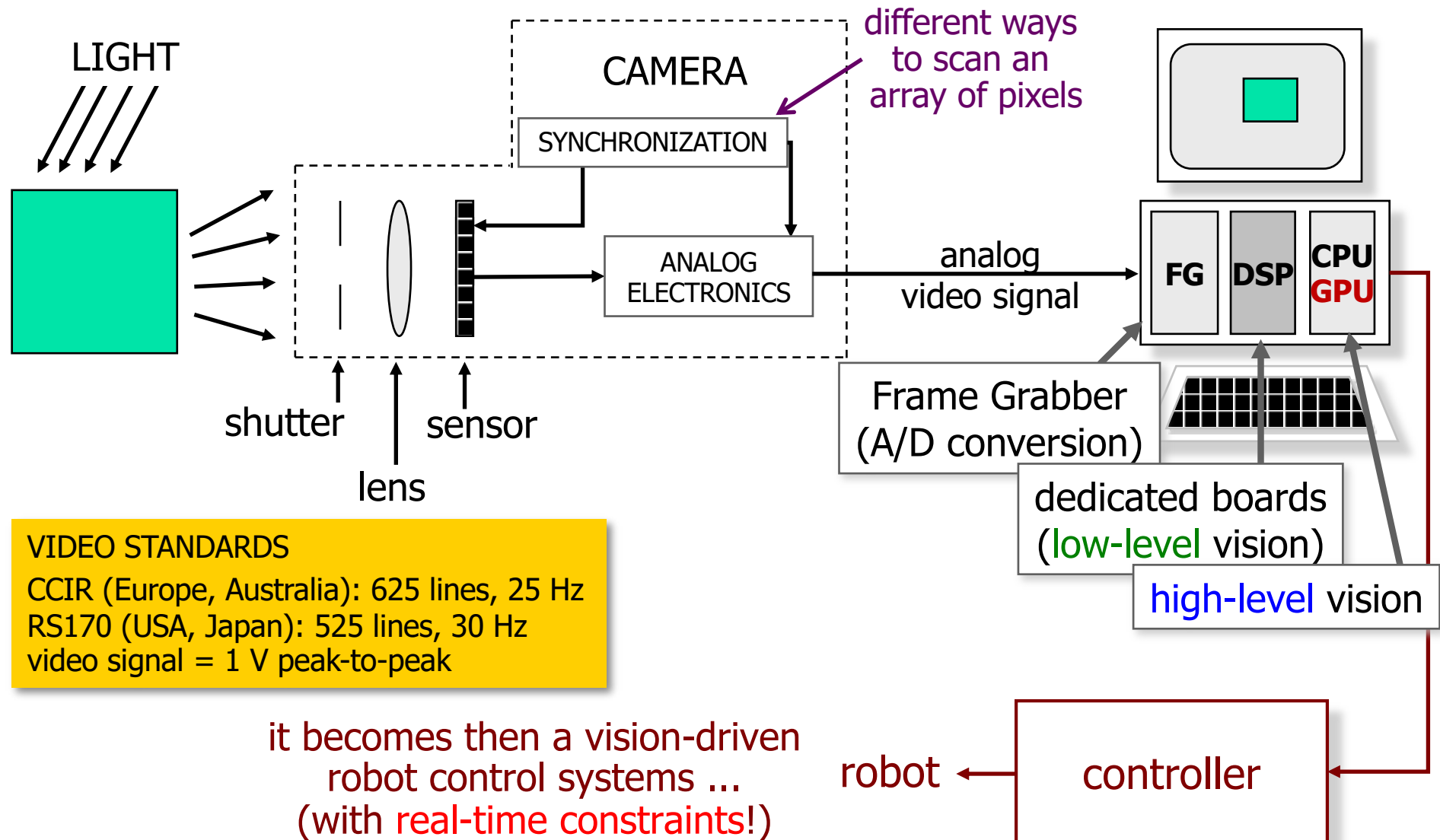


video





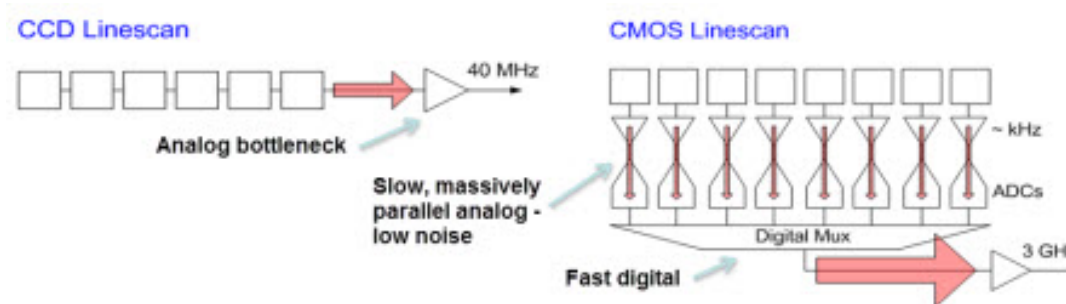
Vision systems





Sensors for vision

- arrays (spatial sampling) of photosensitive elements (**pixel**) converting light energy into electrical energy
- **CCD** (Charge Coupled Device): each pixel surface is made by a semiconductor device, **accumulating** free charge when hit by photons (**photoelectric effect**); “integrated” charges “read-out” by a sequential process (external circuitry) and transformed into voltage levels
- **CMOS** (Complementary Metal Oxide Semiconductor): each pixel is a **photodiode**, directly providing a voltage or current proportional to the **instantaneous** light intensity, with possibility of random access to each pixel





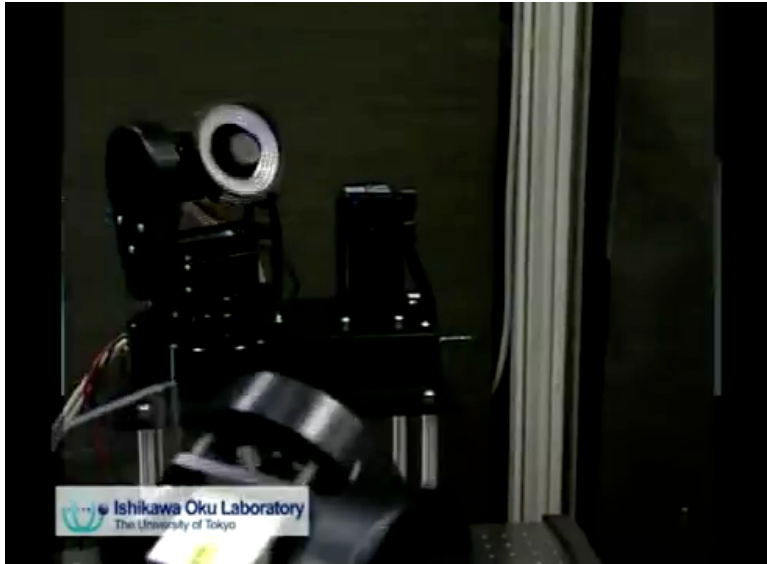
CMOS versus CCD

- reduction of fabrication costs of CMOS imagers
- better spatial resolution of elementary sensors
 - CMOS: 1M pixel, CCD: 768×576 pixel
- faster processing speed
 - 1000 vs. 25 fps (frames per second)
- possibility of integrating “intelligent” functions on single chip
 - sensor + frame grabber + low-level vision
- random access to each pixel or area
 - flexible handling of ROI (Region Of Interest)
- possibly lower image quality w.r.t. CCD imagers
 - sensitivity, especially for applications with low S/N signals
- customization for small volumes is more expensive
 - CCD cameras have been since much longer time on the market

Fast image processing for fast motion control



video



video



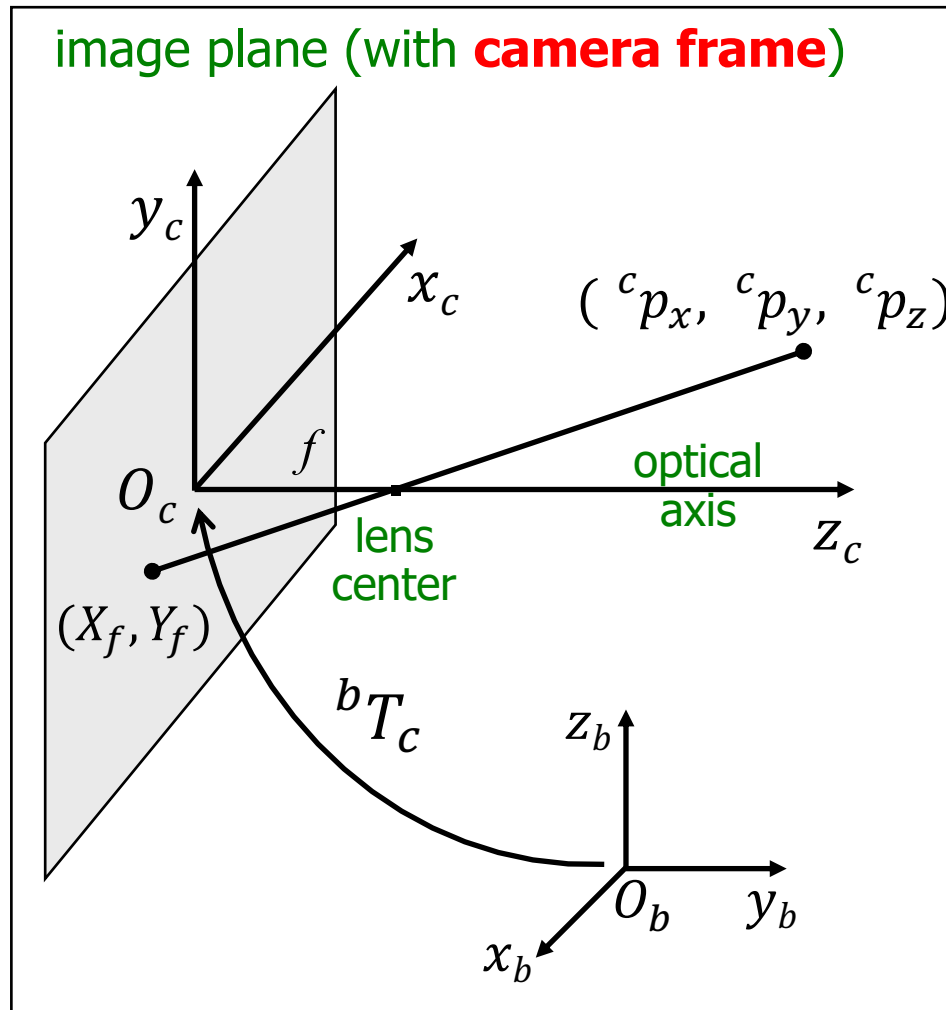
- 1 KHz vision frame rate
 - 1 KHz robot control rate
- @ Ishikawa Lab – U Tokyo
(2007-09)

video





Perspective transformation with pinhole camera model



1. in metric units

$$X_f = \frac{f \cdot {}^c p_x}{f - {}^c p_z} \quad Y_f = \frac{f \cdot {}^c p_y}{f - {}^c p_z}$$

2. in pixel

$$X_I = \frac{\alpha_x f \cdot {}^c p_x}{f - {}^c p_z} + X_0$$

$$Y_I = \frac{\alpha_y f \cdot {}^c p_y}{f - {}^c p_z} + Y_0$$

pixel/metric scaling factor

3. LINEAR MAP in homogeneous coordinates

$$X_I = \frac{x_I}{z_I} \quad Y_I = \frac{y_I}{z_I} \quad \rightarrow \quad \begin{bmatrix} x_I \\ y_I \\ z_I \end{bmatrix} = \Omega \begin{bmatrix} {}^c p_x \\ {}^c p_y \\ {}^c p_z \\ 1 \end{bmatrix}$$

$$\Omega = \begin{bmatrix} \alpha_x & 0 & X_0 & 0 \\ 0 & \alpha_y & Y_0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -1/f & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

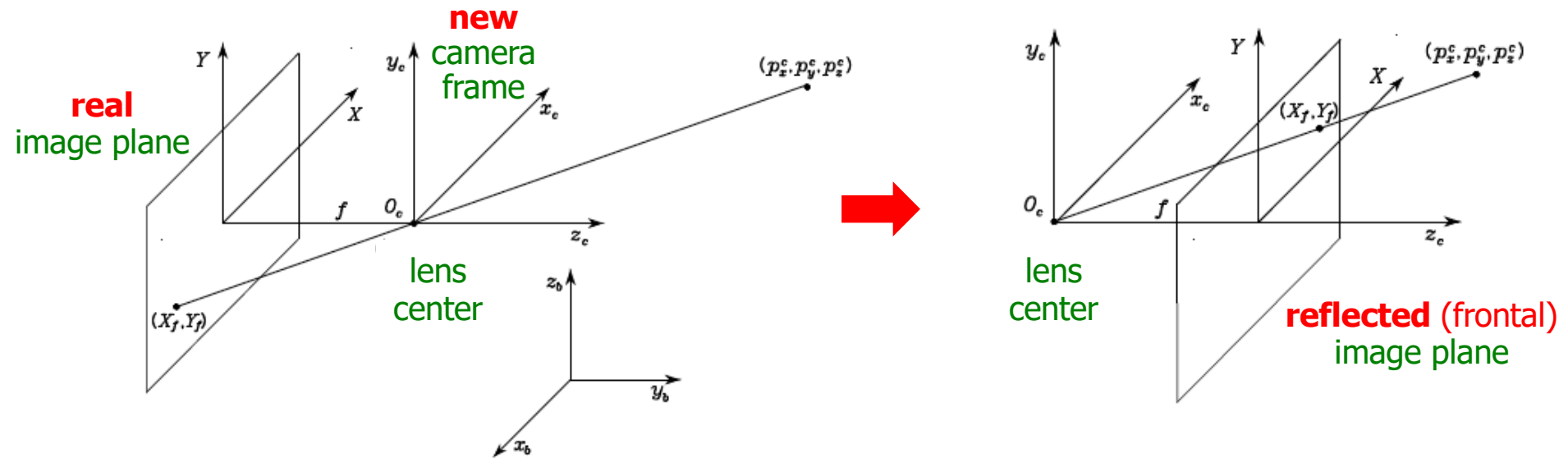
calibration matrix

$$H = \Omega \cdot {}^c T_b$$

intrinsic and extrinsic parameters



Perspective transformation with camera frame at the lens center



1. in metric units

$$X_f = -\frac{f^c p_x}{c p_z} \quad Y_f = -\frac{f^c p_y}{c p_z} \quad \rightarrow \quad X_f = \frac{f^c p_x}{c p_z} \quad Y_f = \frac{f^c p_y}{c p_z}$$

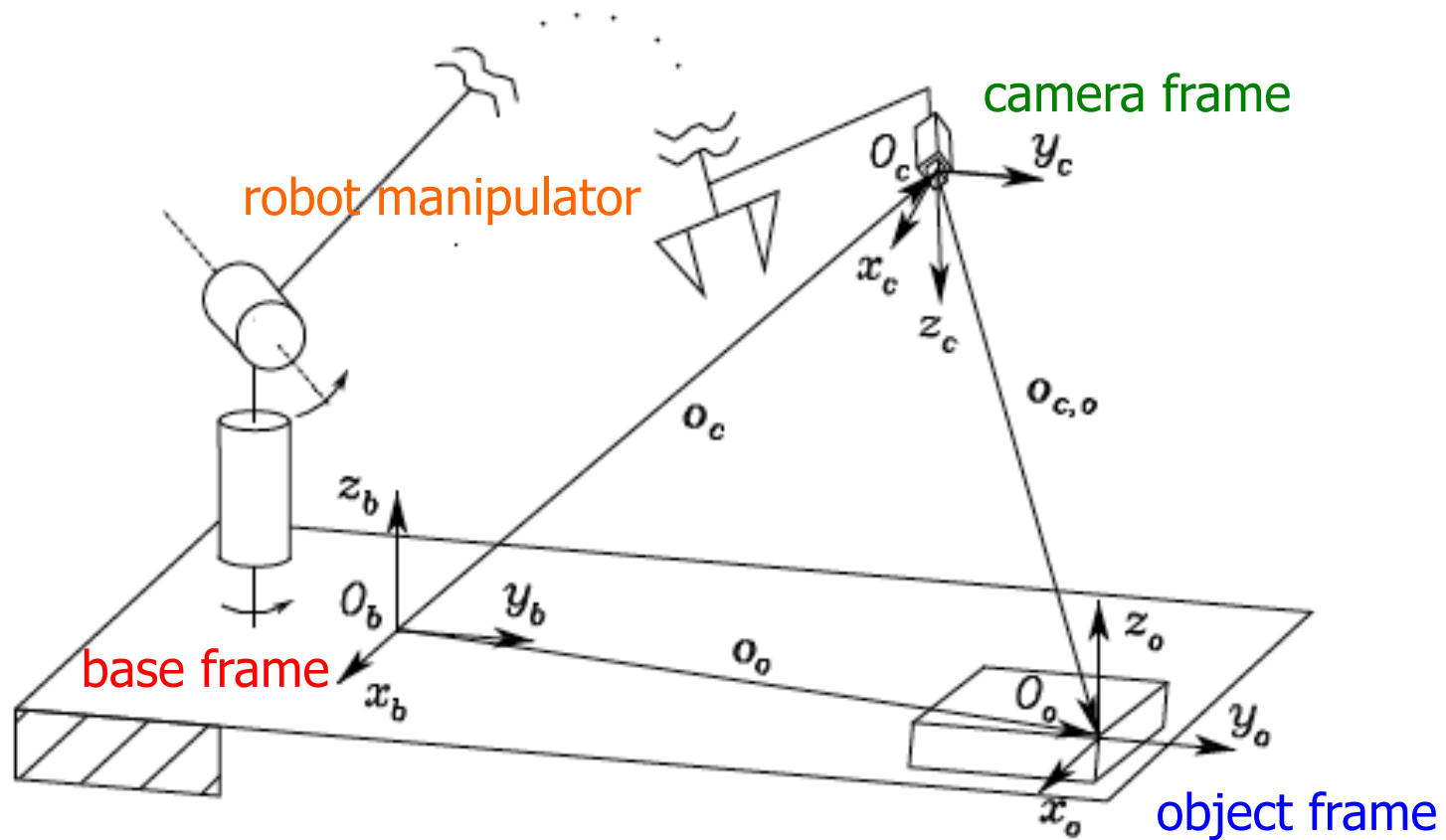
2. in pixel

$$\dots \quad \rightarrow \quad X_I = \frac{\alpha_x f^c p_x}{c p_z} + X_0 \quad Y_I = \frac{\alpha_y f^c p_y}{c p_z} + Y_0$$

3. LINEAR MAP in homogeneous coordinates

$$\dots \quad \rightarrow \quad \begin{bmatrix} x_I \\ y_I \\ z_I \end{bmatrix} = \Omega \begin{bmatrix} c p_x \\ c p_y \\ c p_z \\ 1 \end{bmatrix} \quad \Omega = \begin{bmatrix} \alpha_x f & 0 & X_0 & 0 \\ 0 & \alpha_y f & Y_0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$$

Eye-in-hand camera



Relevant reference frames for visual-based tasks

Kinect

camera + structured light 3D sensor



- RGB camera (with 640×480 pixel)
- depth sensor (by PrimeSense)
 - infrared laser emitter
 - infrared camera (with 320×240 pixel)
- 30 fps data rate
- range: $0.5 \div 5$ m
- depth resolution: $1\text{cm}@2\text{m}$; $7\text{cm}@5\text{m}$
- cost: < 90 €

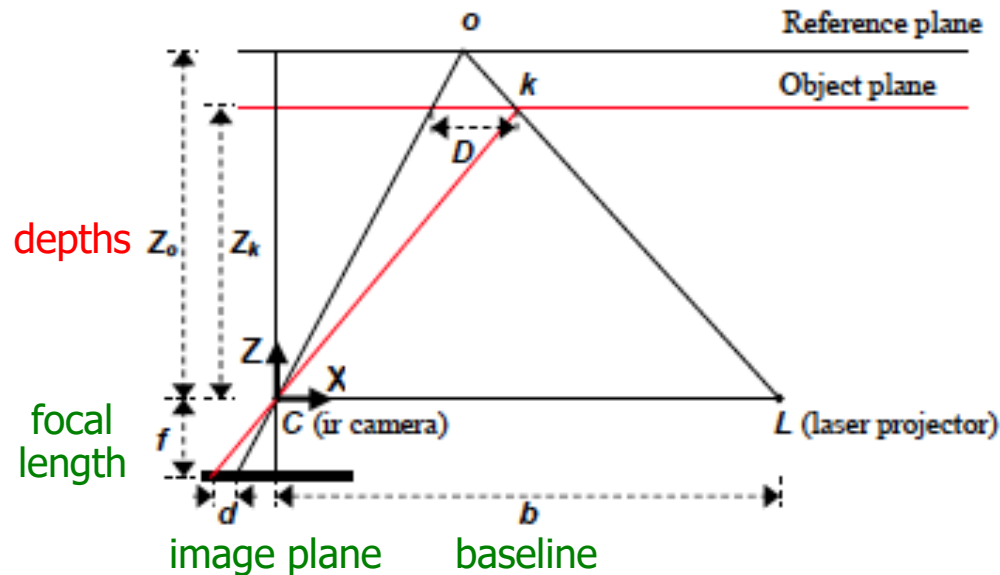


"skeleton" extraction and
human motion tracking



Kinect

Depth sensor operation



- stereo triangulation based on IR source emitting pseudo-random patterns
- reference pattern on IR camera image plane acquired in advance from a plane at known distance and coded in H/W
- correlating the disparity d (10 bits) of reference and received object patterns provides the object depth z_k

1. triangulation equations (by similarity of triangles)

$$\frac{D}{b} = \frac{z_0 - z_k}{z_0} \quad \& \quad \frac{d}{f} = \frac{D}{z_k} \quad \Rightarrow \quad z_k = \frac{z_0}{1 + \frac{d}{fb} z_0}$$

$\Rightarrow x_k = -\frac{z_k}{f} (X_k - X_0 + \delta X)$
 $\Rightarrow y_k = -\frac{z_k}{f} (Y_k - Y_0 + \delta Y)$

2. accurate calibration of sensor

baseline length b , depth of reference z_0 + camera intrinsic parameters (focal length f , lens distortion coefficients $\delta X, \delta Y$, center offsets X_0, Y_0)

How Kinect works

(a 2-minute illustration...)

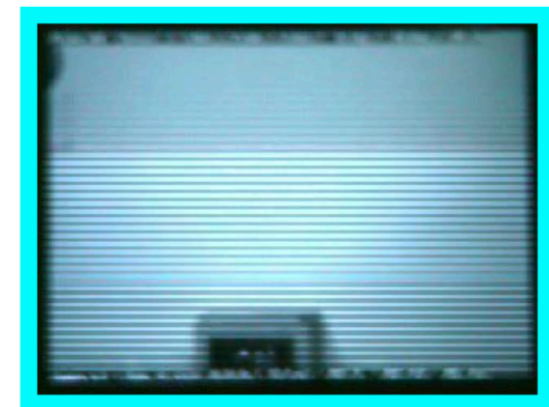
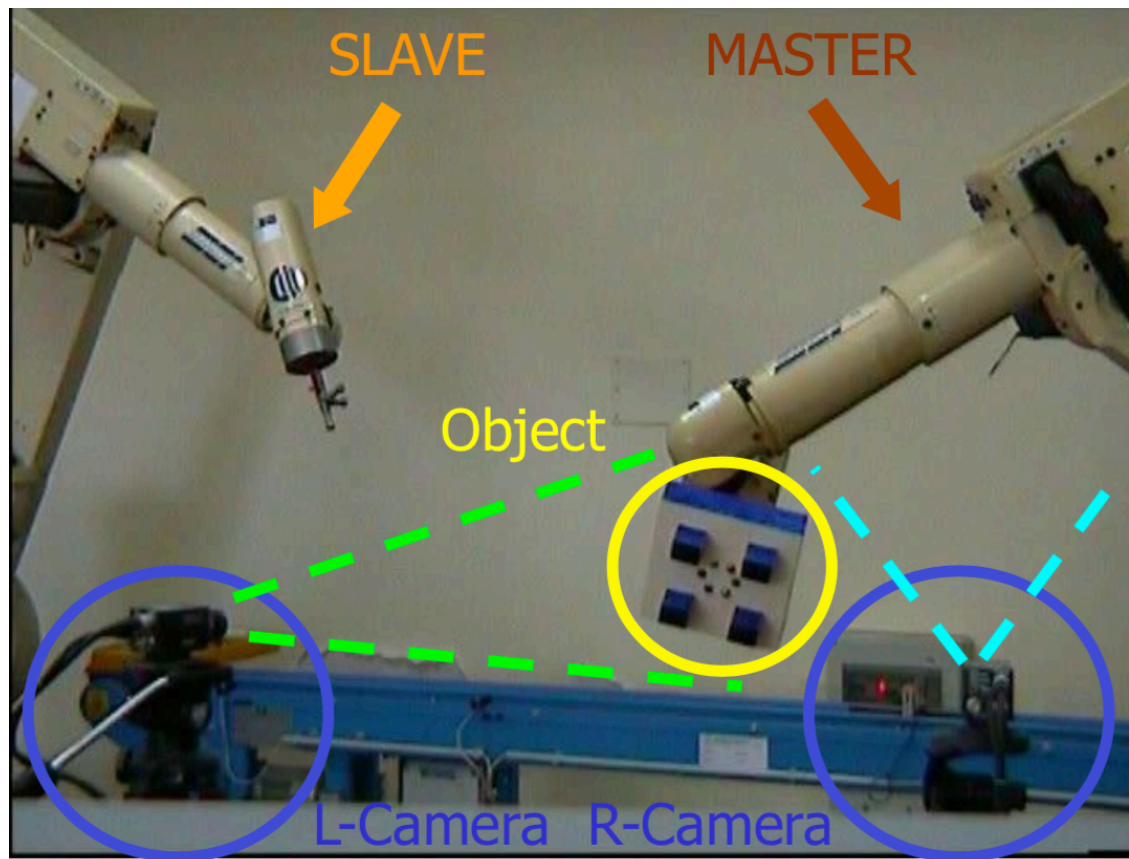


video

<http://youtu.be/uq9SEJxZiUg>

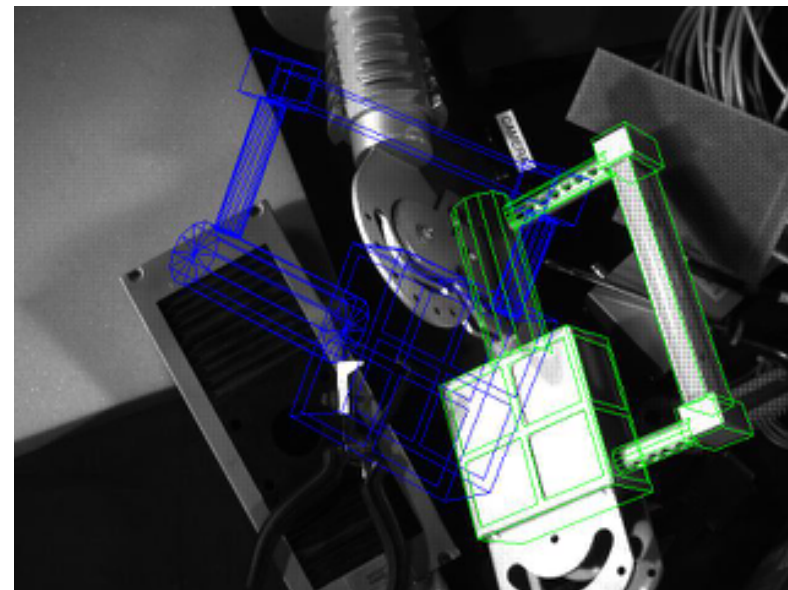
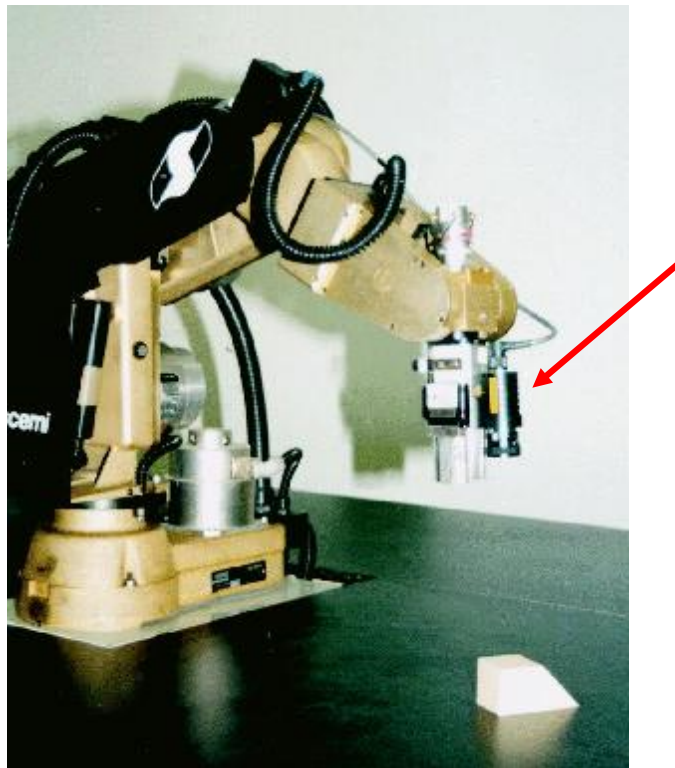
Manipulators and vision systems

- stereovision with two external cameras, fixed in the environment (**eye-to-hand**)



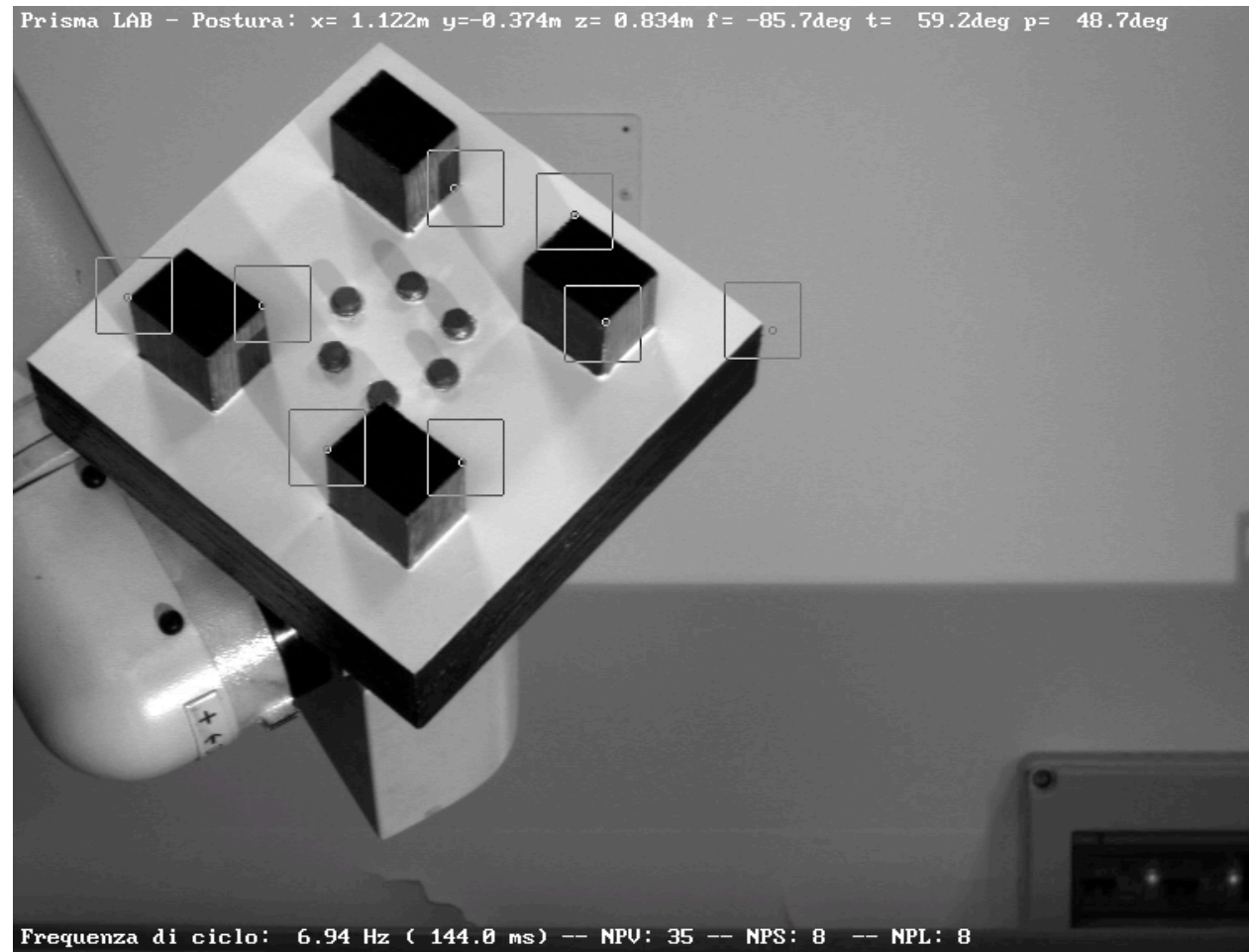
Manipulators and vision systems

- CCD camera mounted on the robot for controlling the end-effector positioning (**eye-in-hand**)





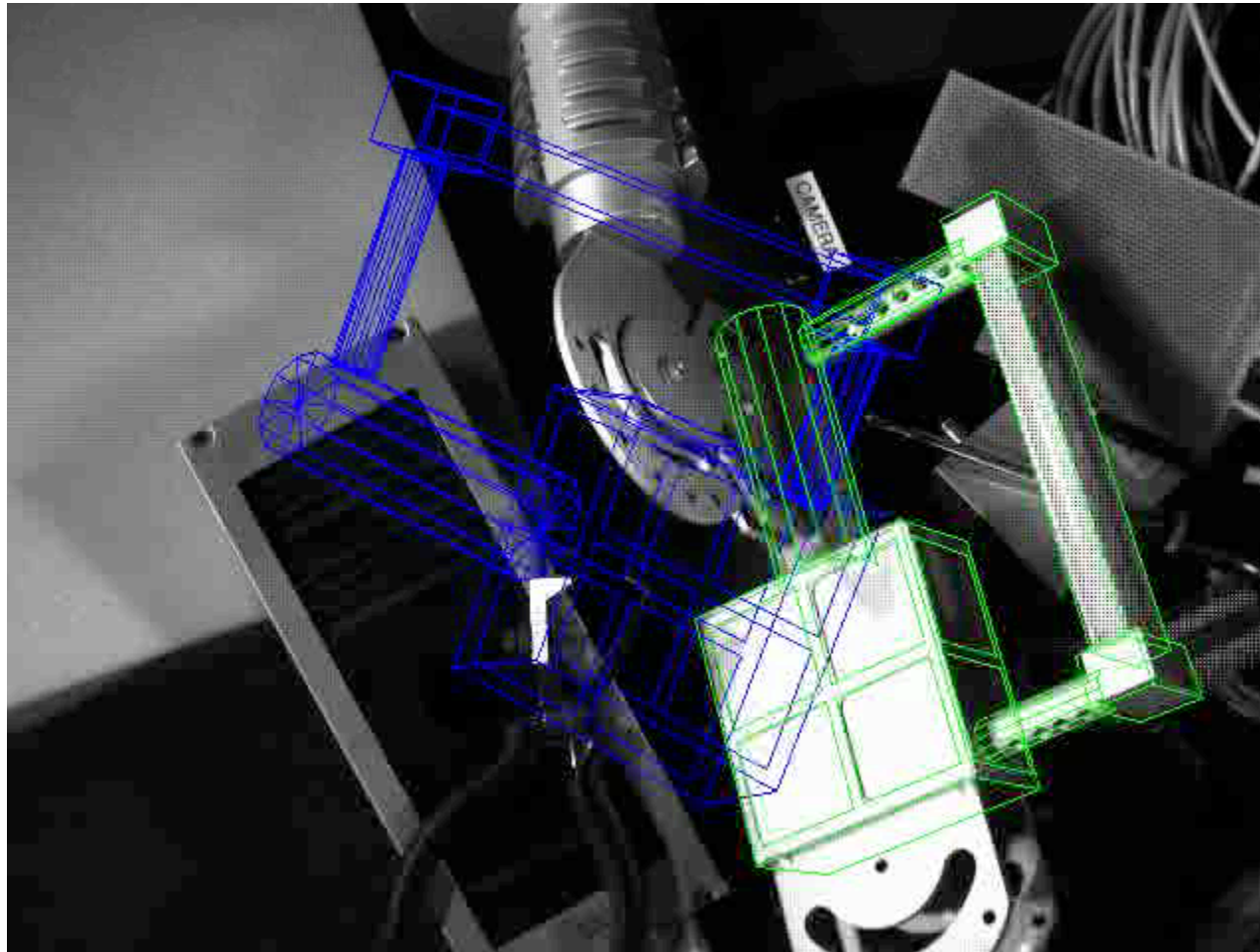
Visual tracking eye-to-hand



video

COMAU robot with position-based 6D tracking from external camera
(DIS, Università di Napoli Federico II)

Visual servoing eye-in-hand

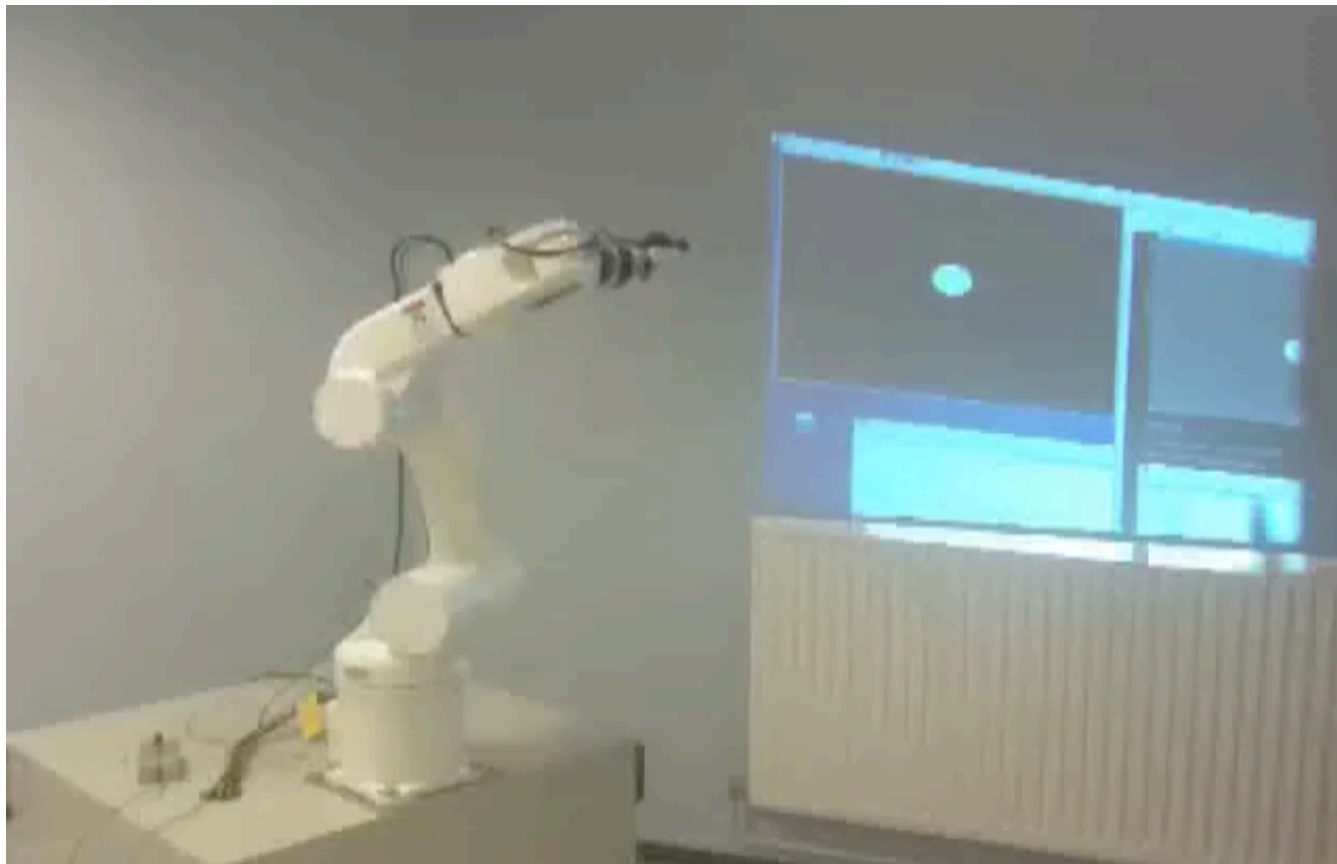


video

Image-based servoing with camera mounted on the robot end-effector
(IRISA/INRIA, Rennes)



Visual servoing and redundancy



video

visual servoing of circle feature ($m = 3: p_x, p_y, r$) by Adept Viper robot ($n = 6$):
redundancy is used for avoiding joint range limits (IRISA/INRIA, Rennes)



Combined visual/force assembly



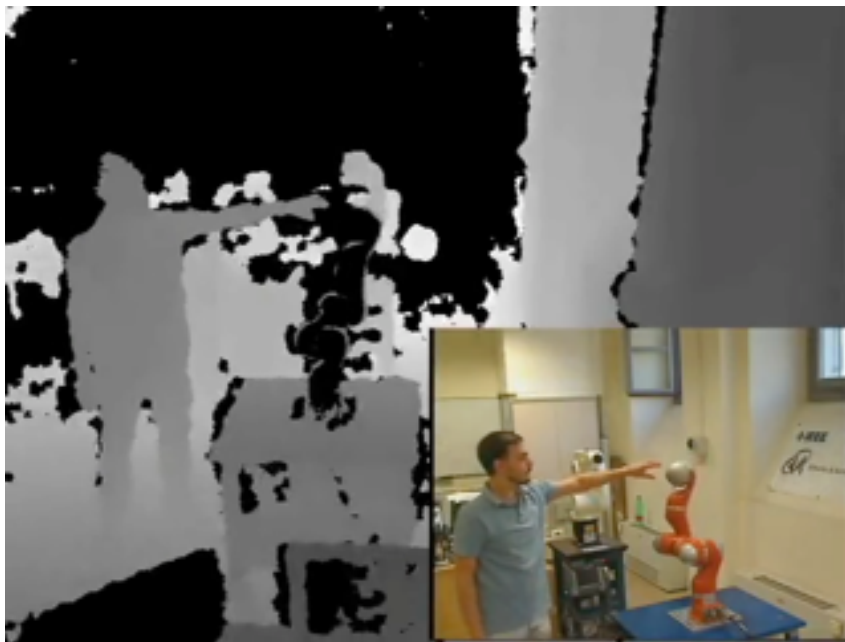
video

KUKA LWR with eye-in-hand camera and F/T sensor
(DLR, IEEE ICRA'07 demo in Roma)

On-line distance computation and human-robot coexistence

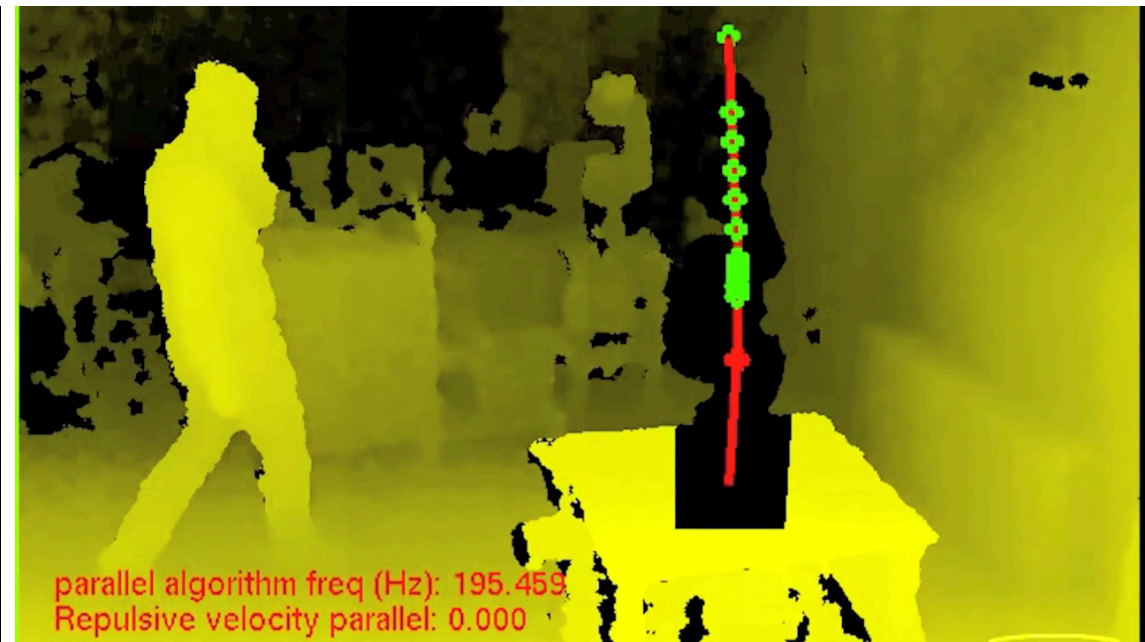


video



monitoring **left-** and **right-** hand
distance to the robot (at same time)

video



several **control points** on robot **skeleton**
used to compute distances and control motion

KUKA LWR with a Kinect monitoring its workspace
(DIAG Robotics Laboratory, EU project SAPHARI, 2013)