



# ***EuRoC Project***

***UAV control application for an European Challenge***

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Reconfigurable  
Interactive  
Manufacturing Cell



Shop Floor Logistics  
and Manipulation



Plant Inspection  
And Servicing

# European Robotics Challenges



- **Stage I – QUALIFYING: Simulation Contest**

The simulation contests are ranked according to objective metrics (criteria and grading system). The best 45 contestants ( $3 \times 15$ ) are selected based on their scores in the tests, and they become **Perspective Challengers**.

Prospective challengers are given an opportunity to form teams with system integrators and end users and submit short proposals, of which the best  $3 \times 5$  will be selected to become the official Challenger Teams (03/2015).



- **Stage II – REALISTIC LABS: Benchmarking, free-style and showcase**

Round A (benchmarking + free-style).

Round B (showcase).

Challenger Teams will be ranked according to objective metrics (criteria and grading system).  $3 \times 2$  Challenge Finalists will be selected for the Field Tests stage of each challenge (12/2016).

- **Stage III – FIELD TESTS: Pilot Experiments**

This last stage involves much engineering effort because the general solutions developed during the Realistic Labs stage will be customised for end users and tested on the field. A EuRoC Winner will be selected by the BoJ (12/2017).

- **35 participants (9 italian Universities/Laboratories)**
  - ACTLAB (*Università di Parma*)
  - ARS (*Università del Salento*)
  - CASY (*Università di Bologna*)
  - Laborics PSI (*private*)
  - PEGASUS (*Scuola Superiore Sant'Anna*)
  - Polibrì (*Politecnico di Milano*)
  - Robo-Team (*Campus-Bio-Medico di Roma*)
  - RomaUno (*Università La Sapienza di Roma*)
  - UNIPI (*Università di Pisa*)
- **21 of them submitted a solution**

## Challenge 3 Contestants



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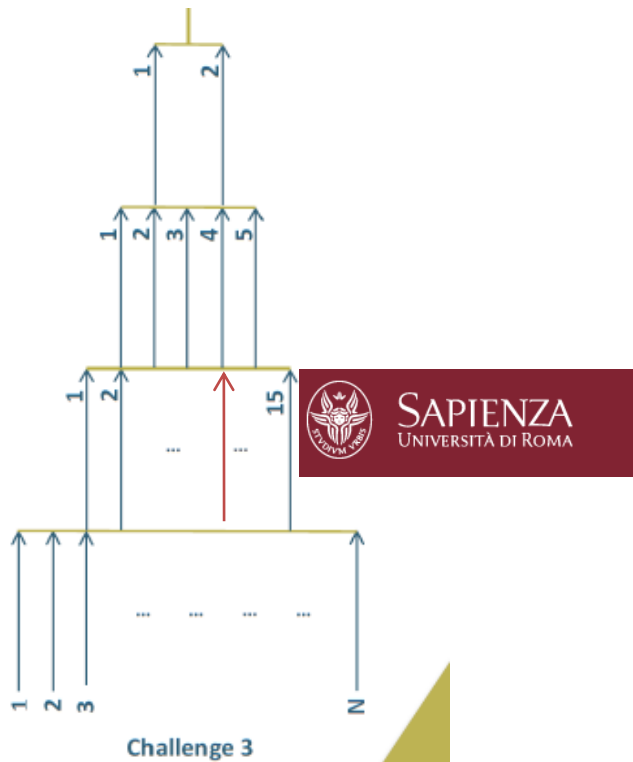


1. ACTLAB
2. Attempto Tuebingen
3. CVG-UPM
4. Eiffel Team
5. Eyefly
6. First ROS Team of Kosice
7. Graz Griffins
8. GRVC-CATEC
9. LEO
10. MIRIAMM
11. NimbRo Copter
12. Polibri
13. proaut-autec
14. Robo-Team
15. RomaUno
16. RPG
17. TUM Flyers
18. Unikorn
19. UNIPI
20. UNIZG-FER
21. Vicomtech-IK4





## The Challenge Chart

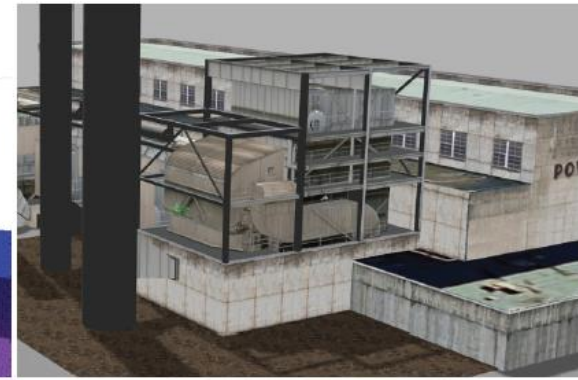
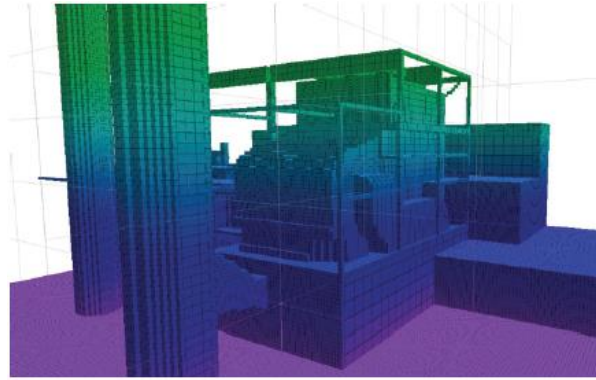


Rank		Team Name	Total Score
1		TUM Flyers	90.5
2		UNIZG-FER	82.5
2		Eiffel Team	82.5
4		NimbRo Copter	77.0
5		RPG	75.0
6		Graz Griffins	74.5
7		MIRIAMM	73.5
8		Attempto Tuebingen	73.0
9		GRVC-CATEC	46.5
10		TU-Chemnitz Proaut	45.0
11		RomaUno	43.0
12		LEO	37.5
13		Polibrì	37.0
14		Unikorn	35.0
15		ACTLAB	25.0

## Challenge 3: Plant Servicing and Inspection



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- Type of robot: Hexacopter MAV
- Track 1: Vision-based localization and reconstruction
  - Task 1
  - Task 2
- Track2: State estimation, control and navigation
  - Task 3
  - Task 4



- Subtask 3.1: simply keep **hovering** at the starting point
  - Subtask 3.2: keep hovering with a **constant wind** applied
  - Subtask 3.3: keep hovering with a **wind gust** applied
- 
- ☐ Some **benchmarks** are defined in each subtask, in order to assign a **score** to the designed solution
  - ☐ Contestants' solutions are designed under **ROS framework** (Robot Operating System)







- MAV System Analysis
- Designed Solution Description
- Simulations & Results

- The robot architecture provided for the Challenge is an **Hexacopter MAV**
- Structure and model comparable to the well-known Quadcopter (six blades instead of **four** ... )
  - Control inputs** are the same: **Thrust** + **torques** on RPY angles
  - Motor velocities mapping** differs because of the number of blades:

## Quadcopter

$$T = f_1 + f_2 + f_3 + f_4$$

$$f_i = b \omega_i^2$$

$$\tau_\varphi = l(f_2 - f_4)$$

$$\tau_{R,i} = d \omega_i^2$$

$$\tau_\vartheta = l(f_1 - f_3)$$

$$\tau_\psi = -\tau_{R,1} + \tau_{R,2} - \tau_{R,3} + \tau_{R,4}$$

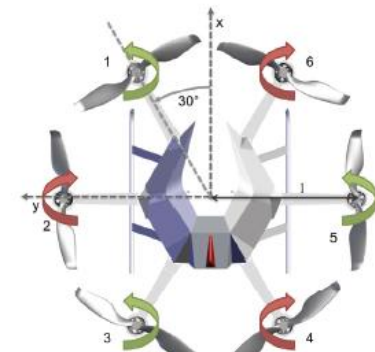


## Hexacopter

$$\begin{bmatrix} \tau_\phi \\ \tau_\theta \\ \tau_\psi \\ T \end{bmatrix} = \text{diag} \left( \begin{bmatrix} b \cdot l \\ b \cdot l \\ d \\ b \end{bmatrix} \right) \cdot \begin{bmatrix} s & 1 & s & -s & -1 & -s \\ -c & 0 & c & c & 0 & -c \\ -1 & 1 & -1 & 1 & -1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix} \cdot \begin{bmatrix} \omega_1^2 \\ \omega_2^2 \\ \omega_3^2 \\ \omega_4^2 \\ \omega_5^2 \\ \omega_6^2 \end{bmatrix}$$

$$s = \sin(30^\circ); \quad c = \cos(30^\circ)$$

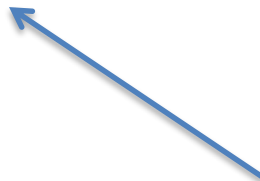
$$l = 0.215 \text{ m}$$



- The MAV model provided is equipped with two **sensors**:
  - A **noisy IMU sensor** providing:
    - *MAV Orientation*
    - *MAV linear acceleration*
    - *MAV angular rate*
  - A **6-DoF Pose sensor** providing:
    - Sensor position
    - Sensor orientation

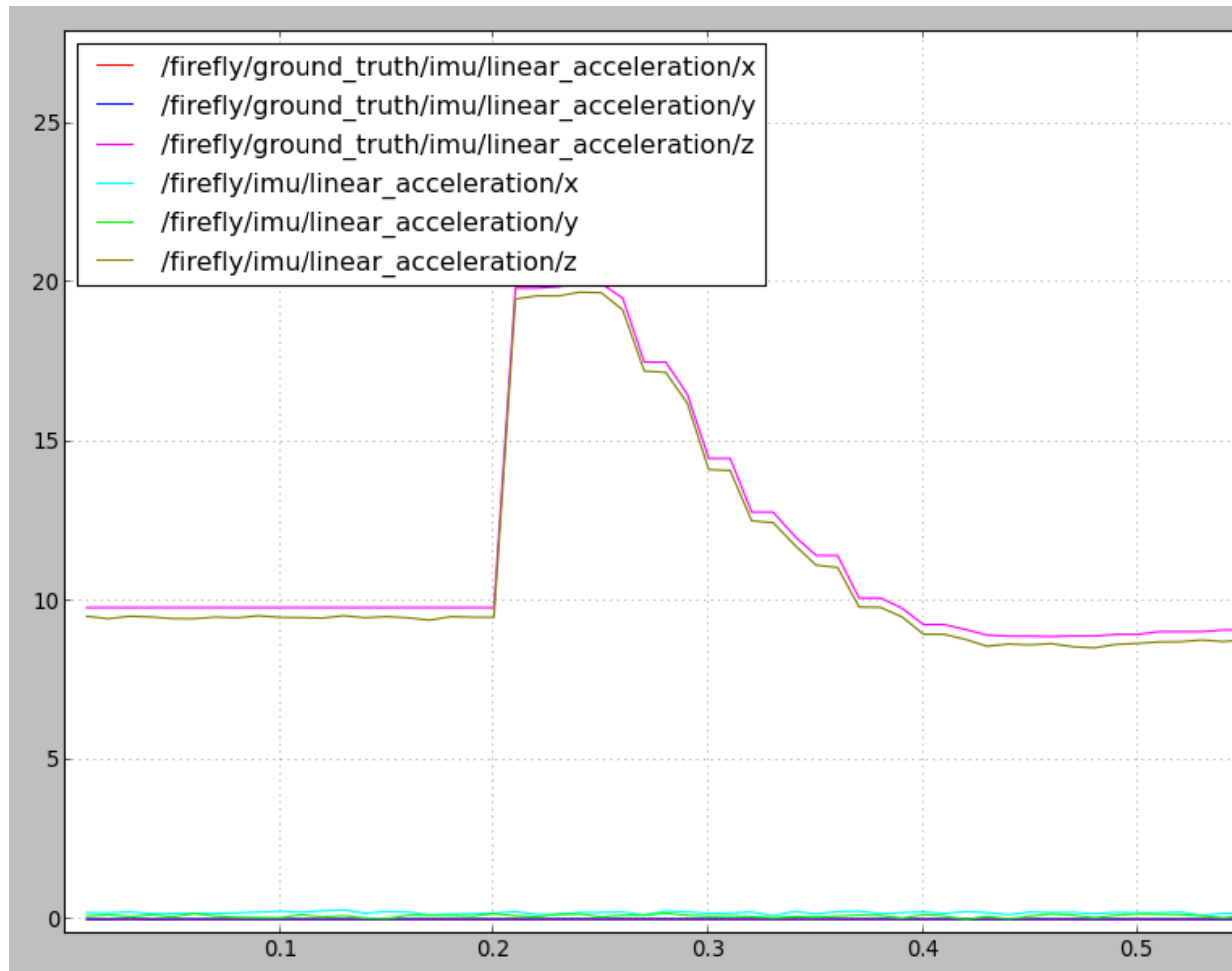


*MAV and Sensor frames  
do **not** coincide!*

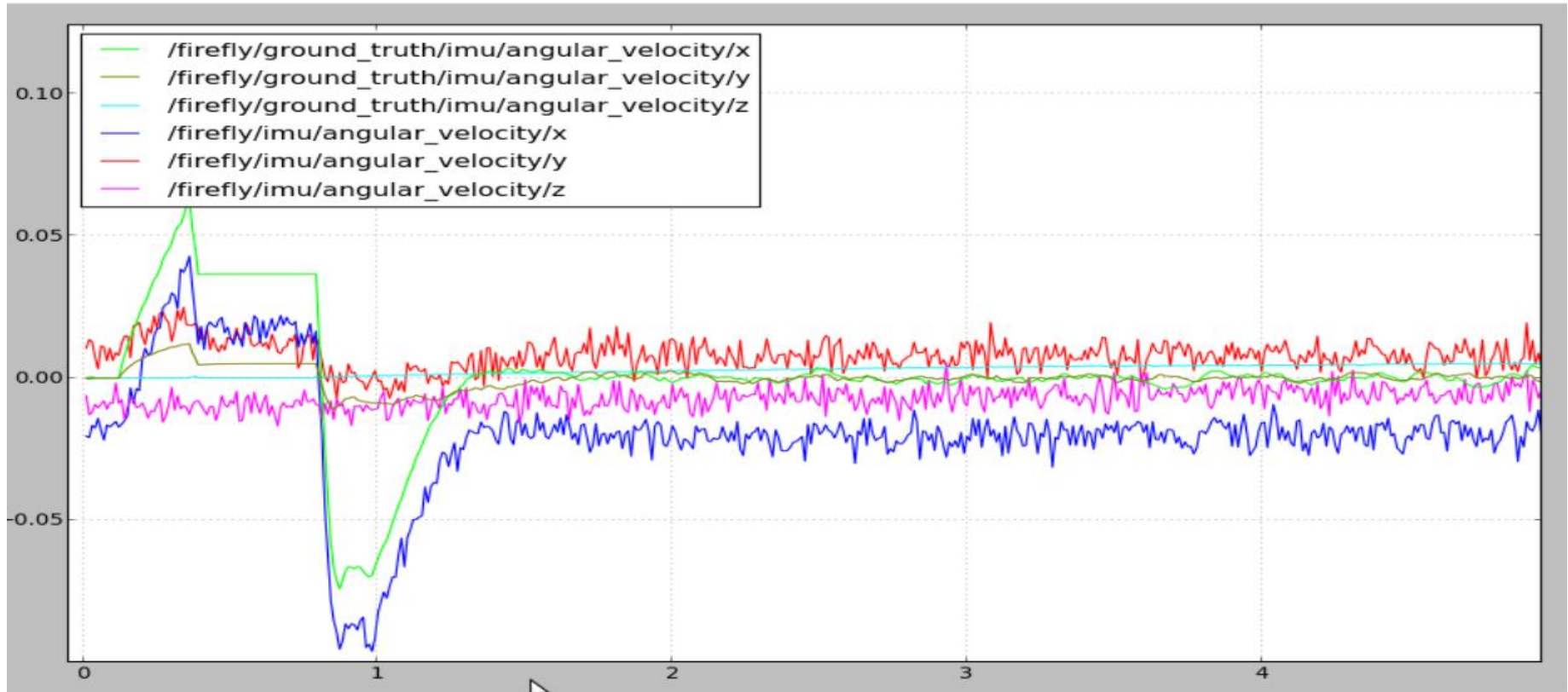


*Not a **real** sensor!  
It abstracts a vision-  
based localization  
approach*

- IMU sensor: *MAV linear acceleration*

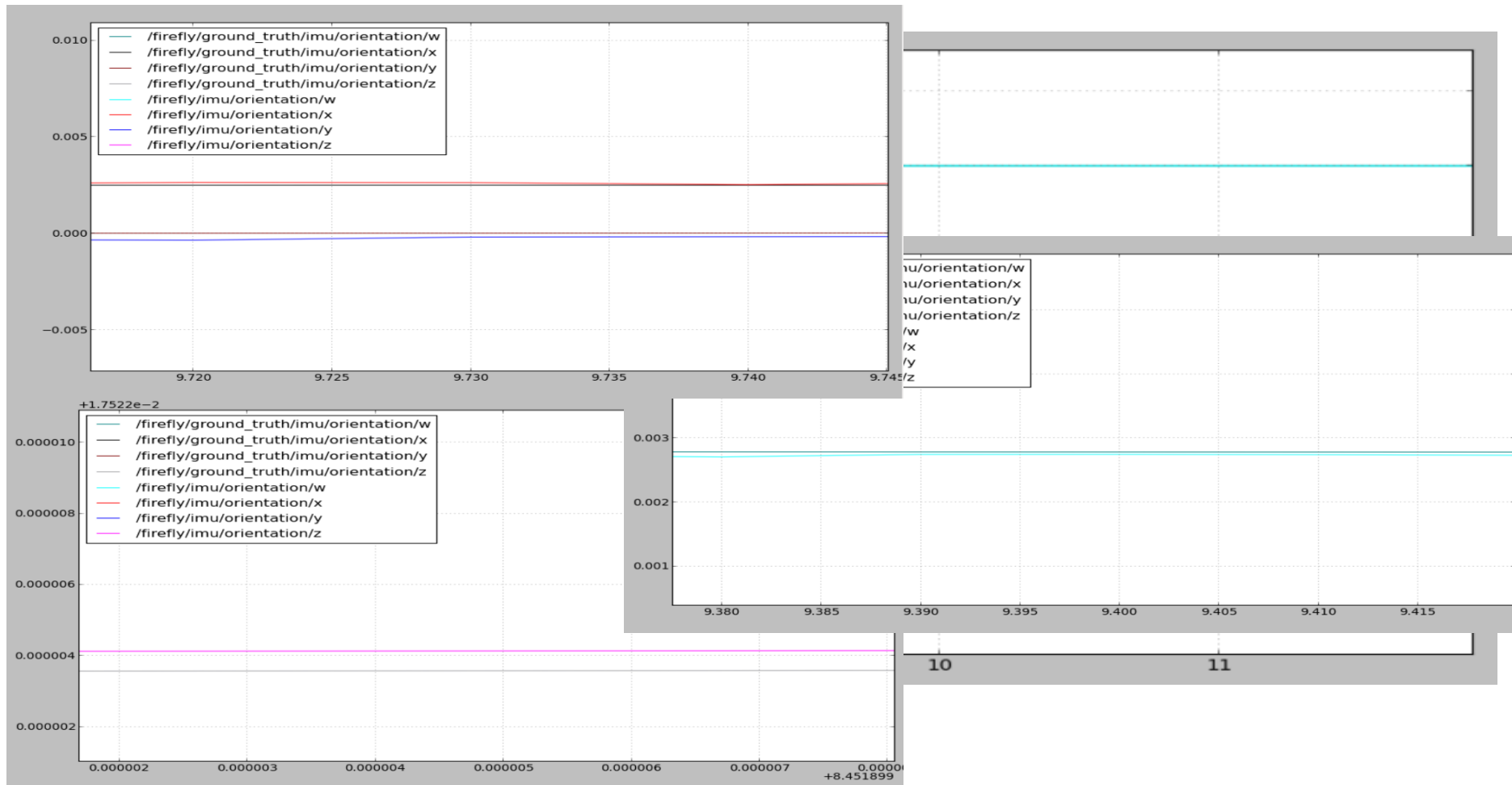


- IMU sensor: *MAV angular rate*

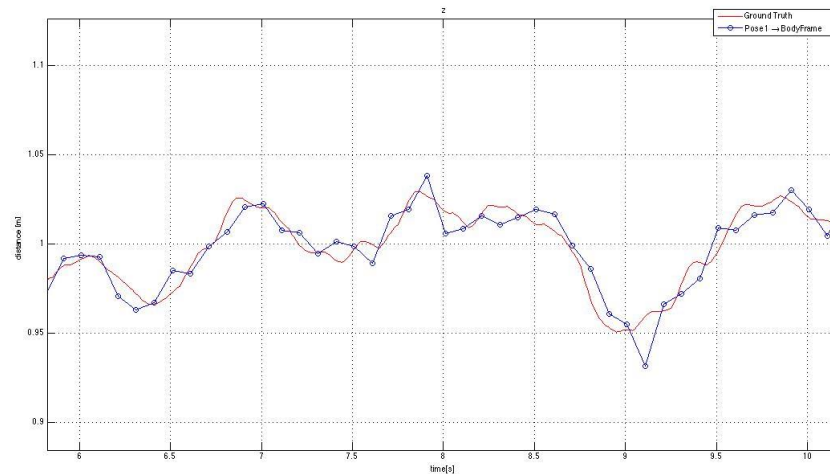
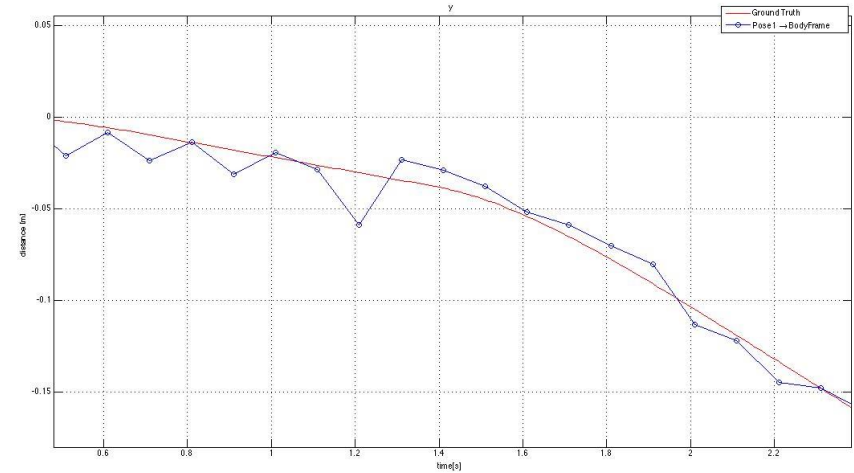
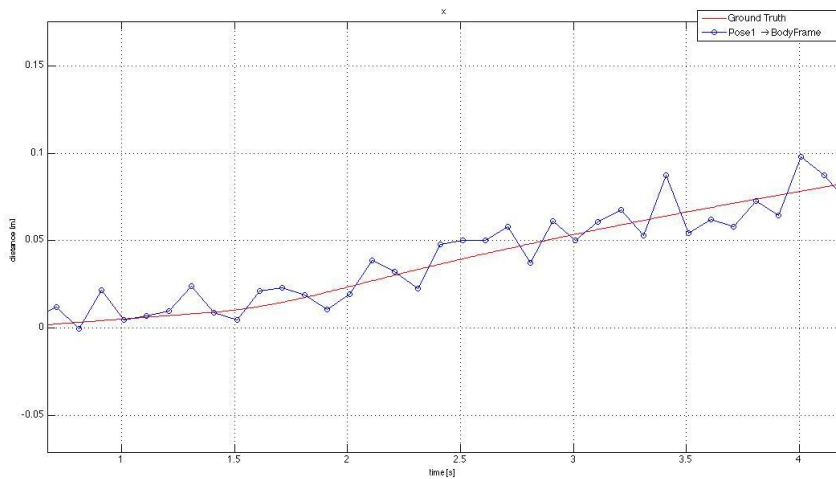




- IMU sensor: *MAV orientation*



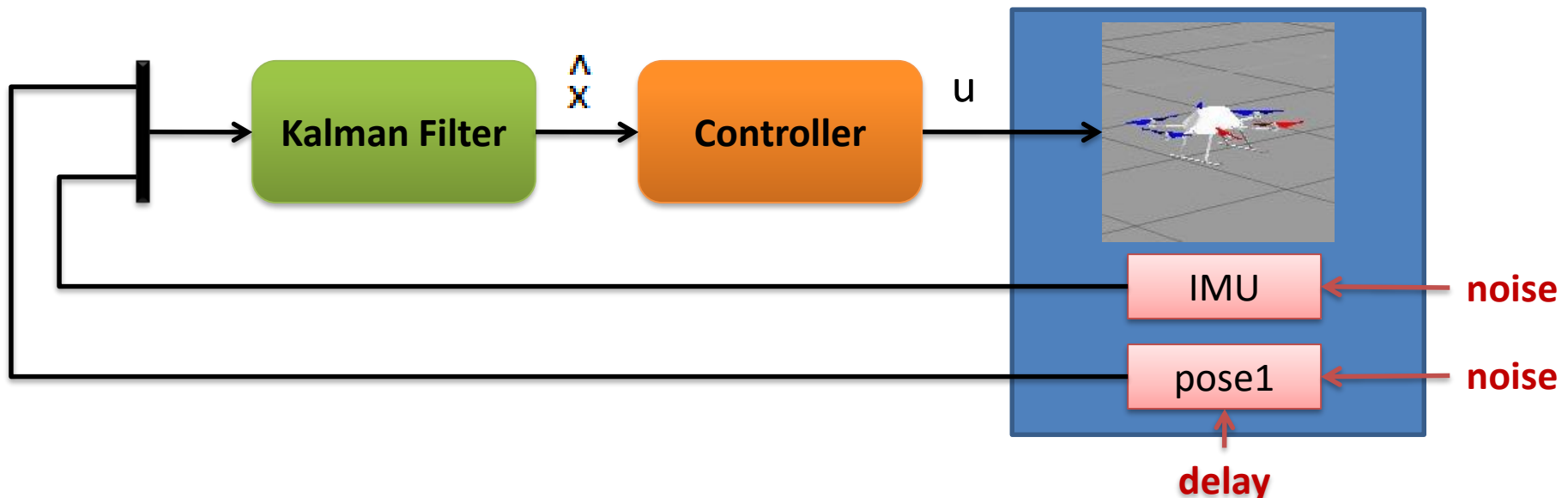
- Pose Sensor



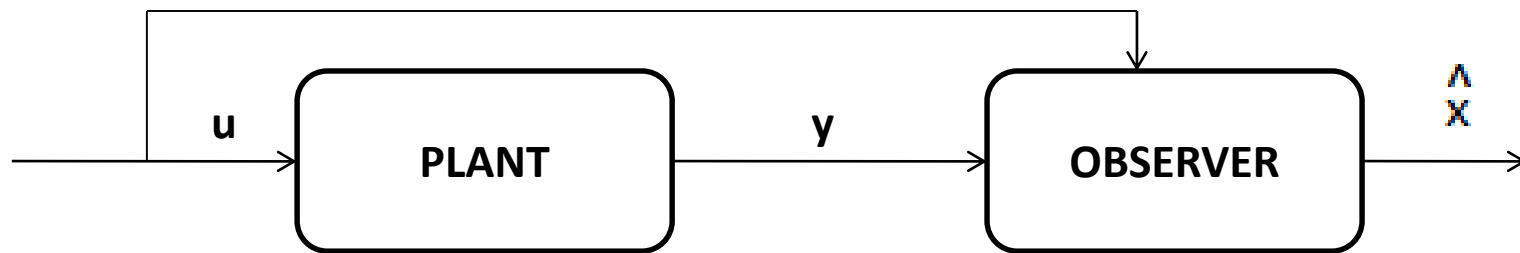


- MAV System Analysis
- Designed Solution Description
- Simulations & Results

- The highly noisy nature of the sensor data prevents us to rawly use them in order to accomplish the assigned control tasks
- A **filter** is usually adopted in order to reject noise coming with corrupted data, so that the control modules are fed with more reliable inputs
- We choose to implement an **Extended Kalman Filter**



- A **Kalman Filter** is an observer that **estimates** the state of a dynamic system, if not directly available



- Built in two steps:
  - Prediction** step: *process dynamics* is used in order to generate an intermediate estimate of the state
  - Update** step: the intermediate estimate is corrected according to the *measured output*





- An **Extended Kalman Filter (EKF)** is an observer for a **non-linear discrete-time system with noise**, with dynamics:

$$\begin{cases} \mathbf{x}_{k+1} = \mathbf{f}_k(\mathbf{x}_k, \mathbf{u}_k) + \mathbf{v}_k \\ \mathbf{y}_k = \mathbf{h}_k(\mathbf{x}_k) + \mathbf{w}_k \end{cases} \quad \begin{aligned} \mathbf{v}_k &\sim \mathcal{N}(0, \mathbf{V}_k) \\ \mathbf{w}_k &\sim \mathcal{N}(0, \mathbf{W}_k) \end{aligned}$$

- State and Covariance Prediction:**

$$\begin{aligned} \hat{\mathbf{x}}_{k+1|k} &= \mathbf{f}_k(\hat{\mathbf{x}}_k, \mathbf{u}_k) \\ \mathbf{P}_{k+1|k} &= \mathbf{F}_k \mathbf{P}_k \mathbf{F}_k^T + \mathbf{V}_k \end{aligned} \quad \mathbf{F}_k = \left. \frac{\partial \mathbf{f}_k}{\partial \mathbf{x}} \right|_{\mathbf{x}=\hat{\mathbf{x}}_k}$$

- State and Covariance Update:**

$$\begin{aligned} \hat{\mathbf{x}}_{k+1} &= \hat{\mathbf{x}}_{k+1|k} + \mathbf{R}_{k+1} \nu_{k+1} \\ \mathbf{P}_{k+1} &= \mathbf{P}_{k+1|k} - \mathbf{R}_{k+1} \mathbf{H}_{k+1} \mathbf{P}_{k+1|k} \end{aligned} \quad \mathbf{H}_{k+1} = \left. \frac{\partial \mathbf{h}_{k+1}}{\partial \mathbf{x}} \right|_{\mathbf{x}=\hat{\mathbf{x}}_{k+1|k}}$$

innovation  $\nu_{k+1} = \mathbf{y}_{k+1} - \mathbf{H}_{k+1} \hat{\mathbf{x}}_{k+1|k}$

Kalman Gain  $\mathbf{R}_{k+1} = \mathbf{P}_{k+1|k} \mathbf{H}_{k+1}^T (\mathbf{H}_{k+1} \mathbf{P}_{k+1|k} \mathbf{H}_{k+1}^T + \mathbf{W}_{k+1})^{-1}$

- The state to be estimated for the hexacopter system is given by:

$$\mathbf{x} = [{}^w\mathbf{p}, {}^w\mathbf{v}, \mathbf{b}_a]^T$$

where:

- ${}^w\mathbf{p}$  is the MAV position in the world frame;
- ${}^w\mathbf{v}$  is the MAV velocity in the world frame;
- $\mathbf{b}_a$  is the accelerometer bias

- Initialization:**

$$\mathbf{x}_0 = \left[ \underbrace{0, 0, 0.08}_{{}^w\mathbf{p}}, \underbrace{0, 0, 0}_{{}^w\mathbf{v}}, \underbrace{0.2, 0.1, -0.3}_{\mathbf{b}_a} \right]^T$$

$$\mathbf{P}_{0|0} = \mathbf{0}_{9 \times 9}$$

$$\mathbf{H}_k = \begin{bmatrix} \mathbf{I}_{3 \times 3} & \mathbf{0}_{3 \times 6} \\ \mathbf{0}_{6 \times 3} & \mathbf{0}_{6 \times 6} \end{bmatrix}$$

$$\mathbf{W}_k = \begin{bmatrix} 0.0001 & 0 & 0 \\ 0 & 0.0001 & 0 \\ 0 & 0 & 0.0001 \end{bmatrix}$$

$$\mathbf{V}_k = \text{diag}(0.00000000016 * \mathbf{I}_{3 \times 3}, \text{diag}(0.00000000016 * \mathbf{I}_{3 \times 3}), \text{diag}(0.00000016 * \mathbf{I}_{3 \times 3}))$$

- An **IMU-based propagation model** has been used: *IMU linear acceleration* and *angular rate* are used as *system inputs* in the **prediction step** (actually only linear acceleration)

$${}^w \hat{\mathbf{p}}_{k+1|k} = {}^w \hat{\mathbf{p}}_k + T_{imu} {}^w \hat{\mathbf{v}}_k + \frac{1}{2} T_{imu}^2 (R(\mathbf{q})a + g)$$

$$a = a_{imu} - \hat{\mathbf{b}}_a$$

## State Prediction

$R(\mathbf{q})$  is the **Rotation matrix** expressing the orientation of the **body frame** wrt the **world frame**

$${}^w \hat{\mathbf{v}}_{k+1|k} = {}^w \hat{\mathbf{v}}_k + T_{imu} (R(\mathbf{q})a + g)$$

$$\hat{\mathbf{b}}_{ak+1|k} = \hat{\mathbf{b}}_{ak}$$

$$\hat{\mathbf{x}}_{k+1|k} = \mathbf{f}_k(\hat{\mathbf{x}}_k, \mathbf{u}_k)$$

$$\frac{\partial {}^w \hat{\mathbf{p}}_{k+1|k}}{\partial {}^w \hat{\mathbf{p}}_k} = \mathbf{I}_{3 \times 3}, \quad \frac{\partial {}^w \hat{\mathbf{p}}_{k+1|k}}{\partial {}^w \hat{\mathbf{v}}_k} = T_{imu} \mathbf{I}_{3 \times 3}, \quad \frac{\partial {}^w \hat{\mathbf{p}}_{k+1|k}}{\partial {}^w \hat{\mathbf{b}}_{ak}} = -\frac{1}{2} T_{imu}^2 R(\mathbf{q}),$$

$$\frac{\partial {}^w \hat{\mathbf{v}}_{k+1|k}}{\partial {}^w \hat{\mathbf{v}}_k} = \mathbf{I}_{3 \times 3}, \quad \frac{\partial {}^w \hat{\mathbf{v}}_{k+1|k}}{\partial {}^w \hat{\mathbf{b}}_{ak}} = -T_{imu} R(\mathbf{q}), \quad \frac{\partial {}^w \hat{\mathbf{b}}_{ak+1|k}}{\partial {}^w \hat{\mathbf{b}}_{ak}} = \mathbf{I}_{3 \times 3},$$

$\mathbf{F}_k$  non-zero entries

$$T_{imu} = 0.01s$$

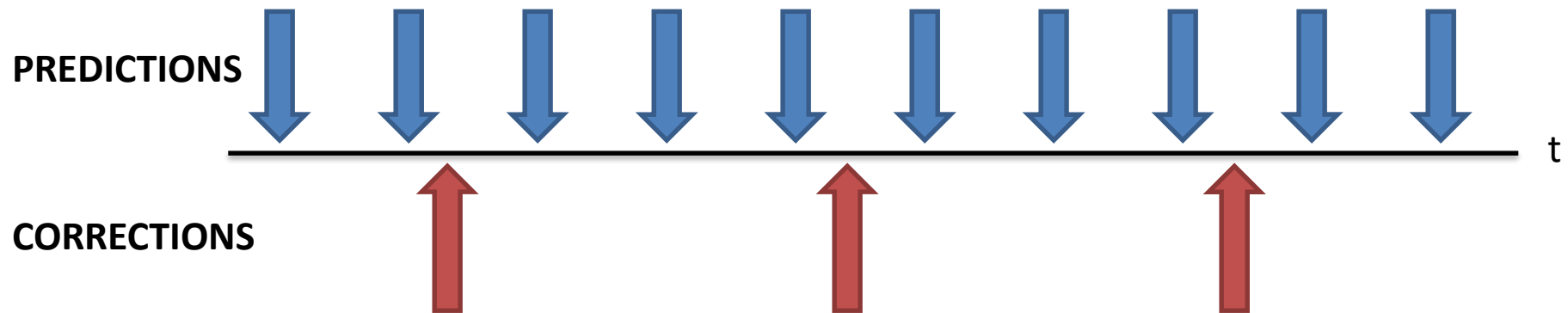
## Covariance Prediction

$$\mathbf{P}_{k+1|k} = \mathbf{F}_k \mathbf{P}_k \mathbf{F}_k^T + \mathbf{V}_k$$

- The Correction step is performed with data coming from the Pose Sensor, where

$$T_{pose} = 0.1s \quad (\neq T_{imu} = 0.01 !!!)$$

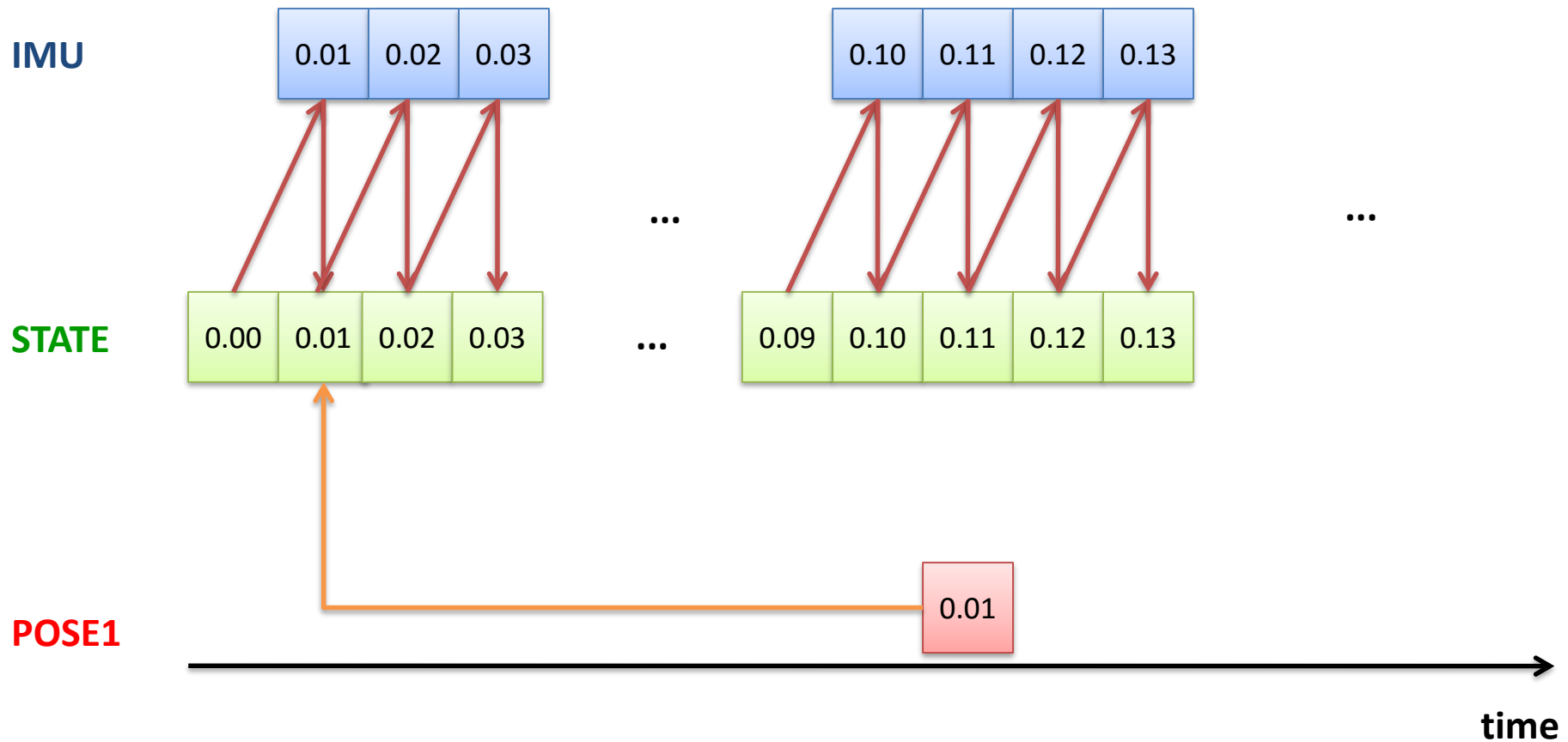
- The Prediction and Correction steps rates are clearly different: the result is that the filter applies a certain number of **predictions** before a new measurement arrives (and so, a **correction** is performed)



- The equations shown before (see State and Covariance Update) are then applied whenever a new Pose sensor message arrives

- In this way, **noise** and **low-rate** issues can be handled in the sensors...
- ... but Pose Sensor is still **delayed!!**
- In fact, Pose Sensor messages contain a *timestamp* field referring to a previous time instant, so the corresponding correction has to be applied on a properly previous prediction
- This does not cause so many troubles while working *off-line*, since a simple *timestamp comparison* is enough in order to apply the correction to the proper intermediate estimate
- On the other hand, when everything needs to work *on-line*, the **validation** on the virtual environment **Gazebo** has to include a **synchronization mechanism ...**

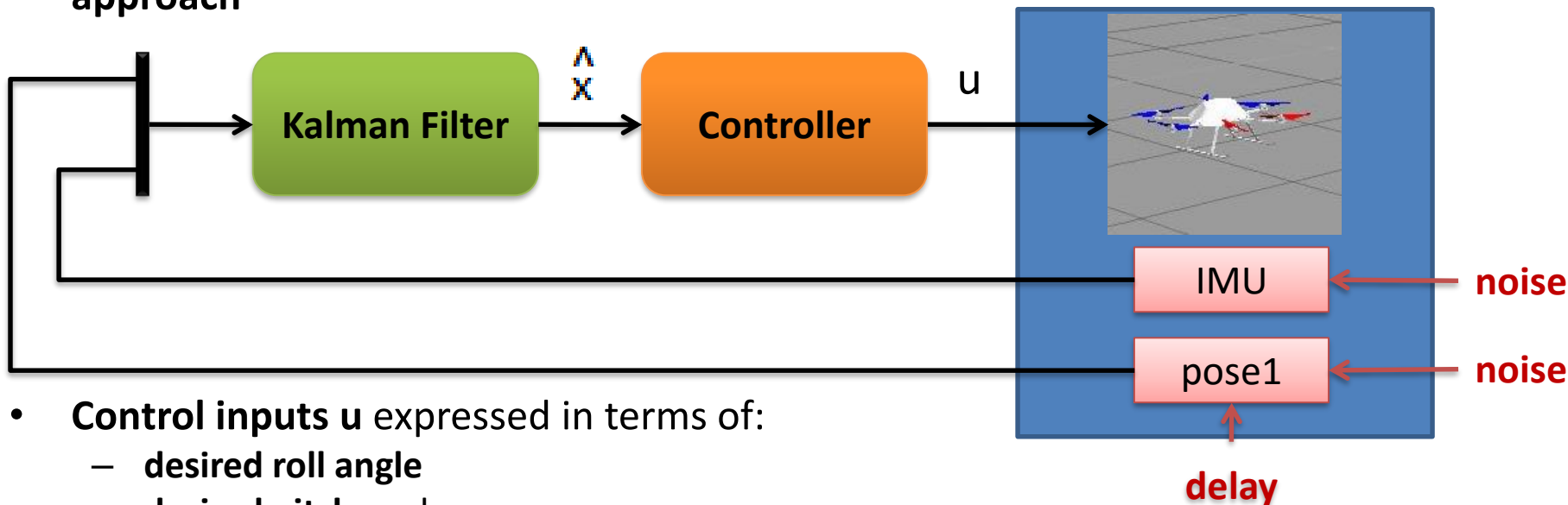




## From filter ... To control

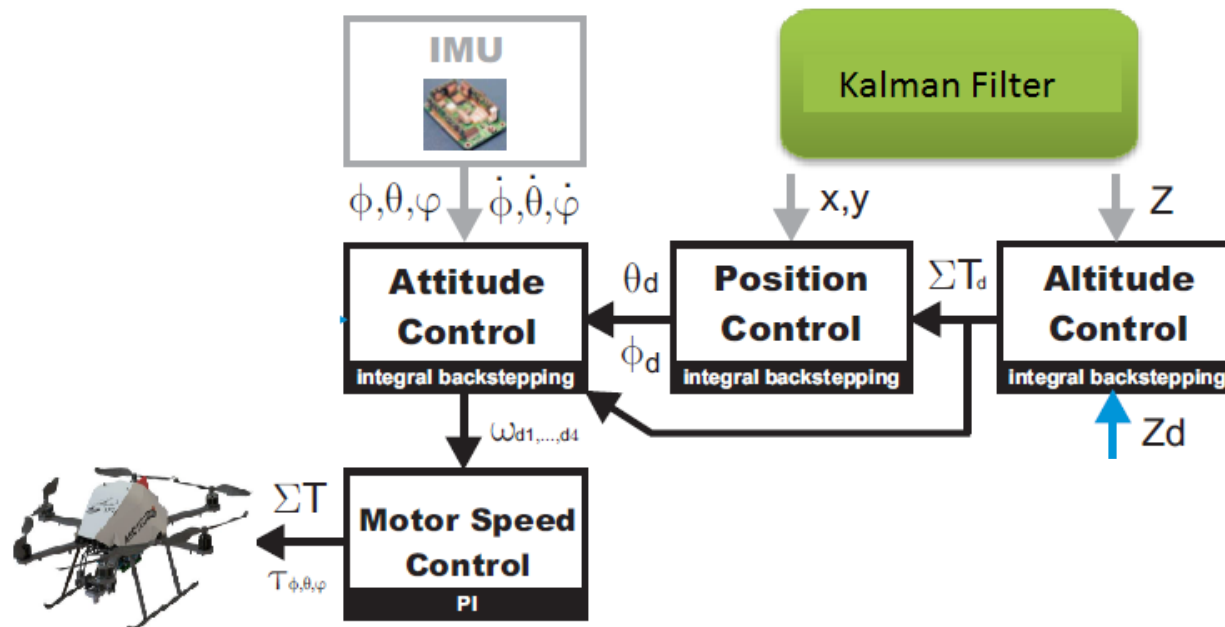


- Data coming from the Kalman Filter module are more reliable to be managed than noisy sensor data
- These data are used in order to feed the **Controller** module that allows the MAV to behave in a desired way by computing proper **control inputs**
- The chosen control paradigm for this application is an **Integral Backstepping approach**



- **Control inputs  $u$**  expressed in terms of:
  - desired roll angle
  - desired pitch angle
  - desired yaw rate
  - Thrust

- **Integral Backstepping** paradigm differentiates three **control modules** for **altitude**, **position** and **attitude**
- In our node:
  - **Altitude** and **Position controller** have been implemented
  - **Attitude controller** is an inner module of the MAV provided by the organizers

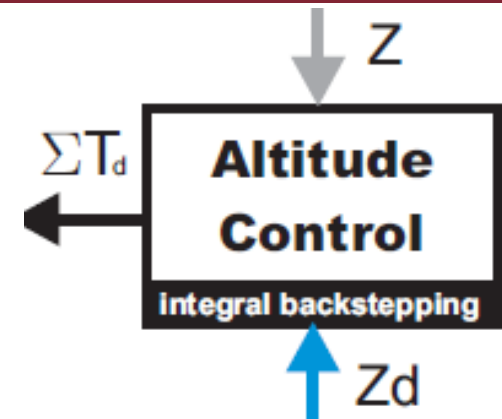


- Altitude tracking error

$$e_z = z_d - z$$

- Altitude speed tracking error

$$e_{\dot{z}} = c_z e_z + \dot{z}_d + \lambda_z \chi_z - \dot{z}$$



$$\chi_i = \int_0^t e_i(\tau) d\tau$$

$$c_z, c_{\dot{z}}, \lambda_z > 0$$

- Thrust** control input

$$T = \frac{m}{\cos \phi \cos \theta} = \left[ g + (1 - c_z^2 + \lambda_z) e_z + (c_z + c_{\dot{z}}) e_{\dot{z}} - c_z \lambda_z \chi_z \right]$$

- x- and y-tracking errors

$$e_x = x_d - x$$

$$e_y = y_d - y$$

- Speed tracking errors

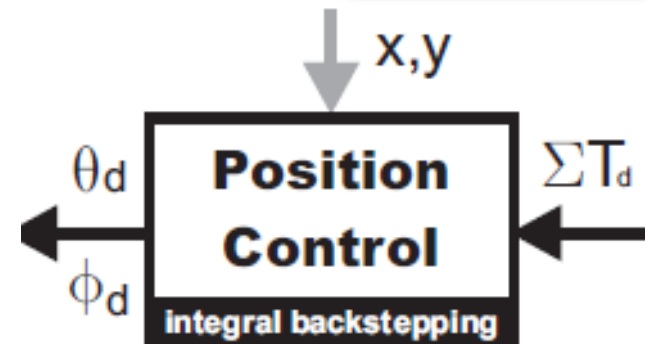
$$e_{\dot{x}} = c_x e_x + \dot{x}_d + \lambda_x \chi_x - \dot{x}$$

$$e_{\dot{y}} = c_y e_y + \dot{y}_d + \lambda_y \chi_y - \dot{y}$$

- desired **roll** and **pitch** angles control inputs

$$\theta_d = \frac{m}{T} \left[ \left( 1 - c_x^2 + \lambda_x \right) e_x + (c_x + c_{\dot{x}}) e_{\dot{x}} - c_x \lambda_x \chi_x \right]$$

$$\phi_d = -\frac{m}{T} \left[ \left( 1 - c_y^2 + \lambda_y \right) e_y + (c_y + c_{\dot{y}}) e_{\dot{y}} - c_y \lambda_y \chi_y \right]$$



- Attitude Controller has been used as provided in the Simulation VM
- Inputs:**  $T, \phi_d, \theta_d, \psi_d$

## Parameter Initialization

$K_p$ : attitude gain

$K_d$ : angular rate gain

$I$ : inertia matrix

$$b = 8.54858 \cdot 10^{-6} \left[ \frac{kg \cdot m}{s^2} \right]$$

$$d = 1.3677 \cdot 10^{-7} \left[ \frac{kg \cdot m^2}{s^2} \right]$$

This makes gain  
tuning independent  
of inertia matrix

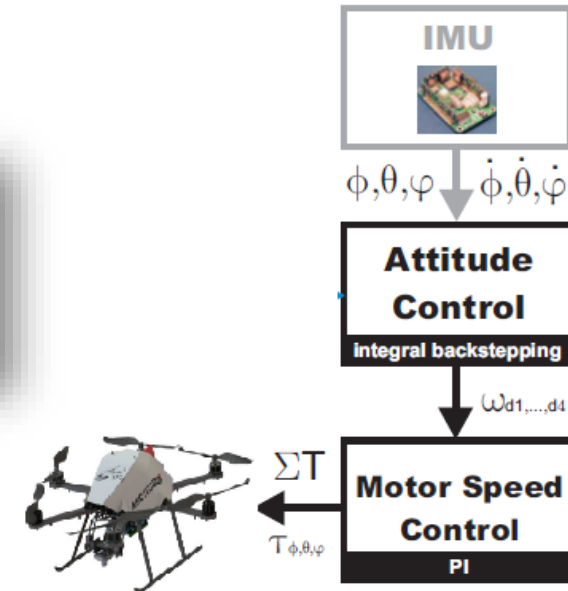
$$\begin{aligned} K_p &\leftarrow K_p / I \\ K_d &\leftarrow K_d / I \end{aligned}$$

$$A = \begin{bmatrix} s & 1 & s & -s & -1 & -s \\ -c & 0 & c & c & 0 & -c \\ -1 & 1 & -1 & 1 & -1 & 1 \\ 1 & 1 & 1 & 1 & 1 & 1 \end{bmatrix} : \text{allocation matrix}$$

$$u = \begin{bmatrix} \tau_\phi \\ \tau_\theta \\ \tau_\psi \\ T \end{bmatrix} \quad K = \text{diag} \left( \begin{bmatrix} b \cdot l \\ b \cdot l \\ d \\ b \end{bmatrix} \right)$$

$$u = K A \omega^2 \rightarrow \omega^2 = (K A)^{-1} u = (K A)^{-1} \begin{bmatrix} I & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} a_\tau \\ T \end{bmatrix}$$

$$\omega^2 = A^T (A A^T)^{-1} K^{-1} \bar{I} a_\tau = \tilde{A} \begin{bmatrix} a_\tau \\ T \end{bmatrix}$$



## Compute Angular Acceleration

$$1. \quad \psi \rightarrow R(\mathbf{q}).\text{get\_yaw}()$$

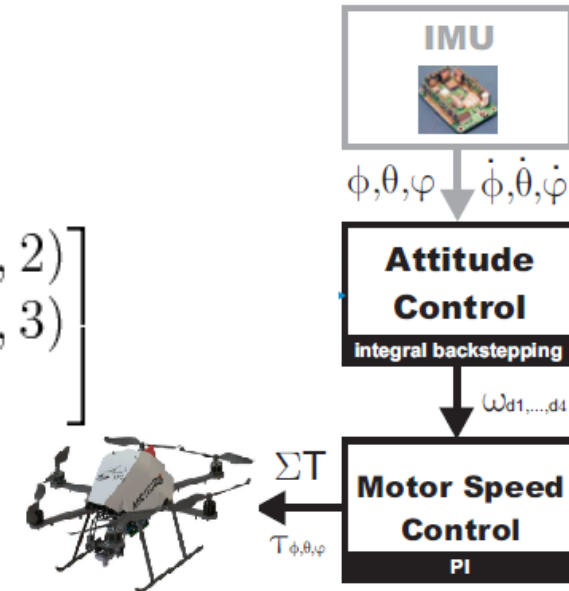
$$2. \quad R_d = R(\psi, \vec{z}) R(\phi_d, \vec{x}) R(\theta_d, \vec{y})$$

$$3. \quad e_R = \frac{1}{2} (R_d^T R - R^T R_d) \rightarrow e_{angle} = \begin{bmatrix} e_R(3, 2) \\ e_R(1, 3) \\ 0 \end{bmatrix}$$

$$4. \quad \omega_d = \begin{bmatrix} 0 \\ 0 \\ \dot{\psi}_d \end{bmatrix}$$

$$5. \quad e_\omega = \omega - R^T R_d \omega_d$$

$$6. \quad a_\tau = -K_p e_{angle} - K_d e_\omega + \omega \times \omega$$





- MAV System Analysis
- Designed Solution Description
- Simulations & Results



- **Two virtual machines** (running Ubuntu 12.04) are provided to each Contestant:
  - A **Simulation VM**, containing the virtual environment (**Gazebo**) for simulations.
  - A **Contestant VM**, containing the Contestant's solution for the assigned tasks.
- The VMs communicate via **Client/Server Protocol**:
  - The **Simulation VM** acts as a **Server** and must not be modified
  - The **Contestant VM** acts as a **Client** submitting the solution to the Server
- **ROS** is installed on both VMS

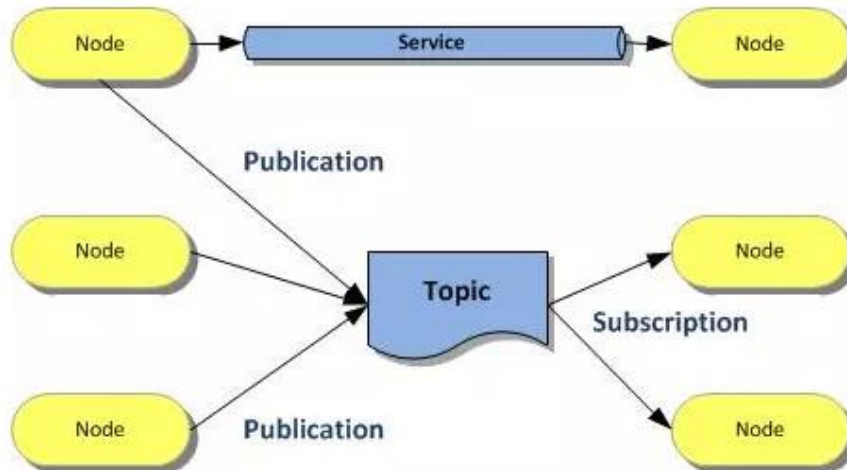


- ROS framework is an Operating System for robots (a *meta-operating system*)
  - **standard OS functionalities** offered:
    - Hardware abstraction
    - Processes handling and message-passing mechanism
    - ...
  - Development environments provided, with client **API libraries**:
    - C++
    - Python
    - Java
    - Lisp

further info: [www.wiki.ros.org](http://www.wiki.ros.org)



- Processes running under ROS are called **nodes**
- **Nodes** communicate through **message-passing mechanism**
- A **message** is a data structure with some designed typed fields (integer, float, boolean, array, ...)
- Nodes can write a message and **publish** it on a **topic**, or it can **subscribe** to a topic in order to read the corresponding message
- A special node, called **roscore**, acts as a **master node** and needs to be run first before any other node.



ROS

- ROS usually works on a single machine; but so ...
- ... How can we make VMs to communicate between them?
- EuRoC partners have set a “*network bridging*” mechanism between the two machines, so that the **roscore** master node of the Server machine is shared with the Client Machine
- On the Contestant VM:

```
i. <host machine's IP>          eurocsimserv  
ii. <Contestant VM adapter 3 IP> eurosimclient
```

```
i. export ROS_MASTER_URI=http://eurocsimserv:11311  
ii. export ROS_HOSTNAME=eurocsimserv
```



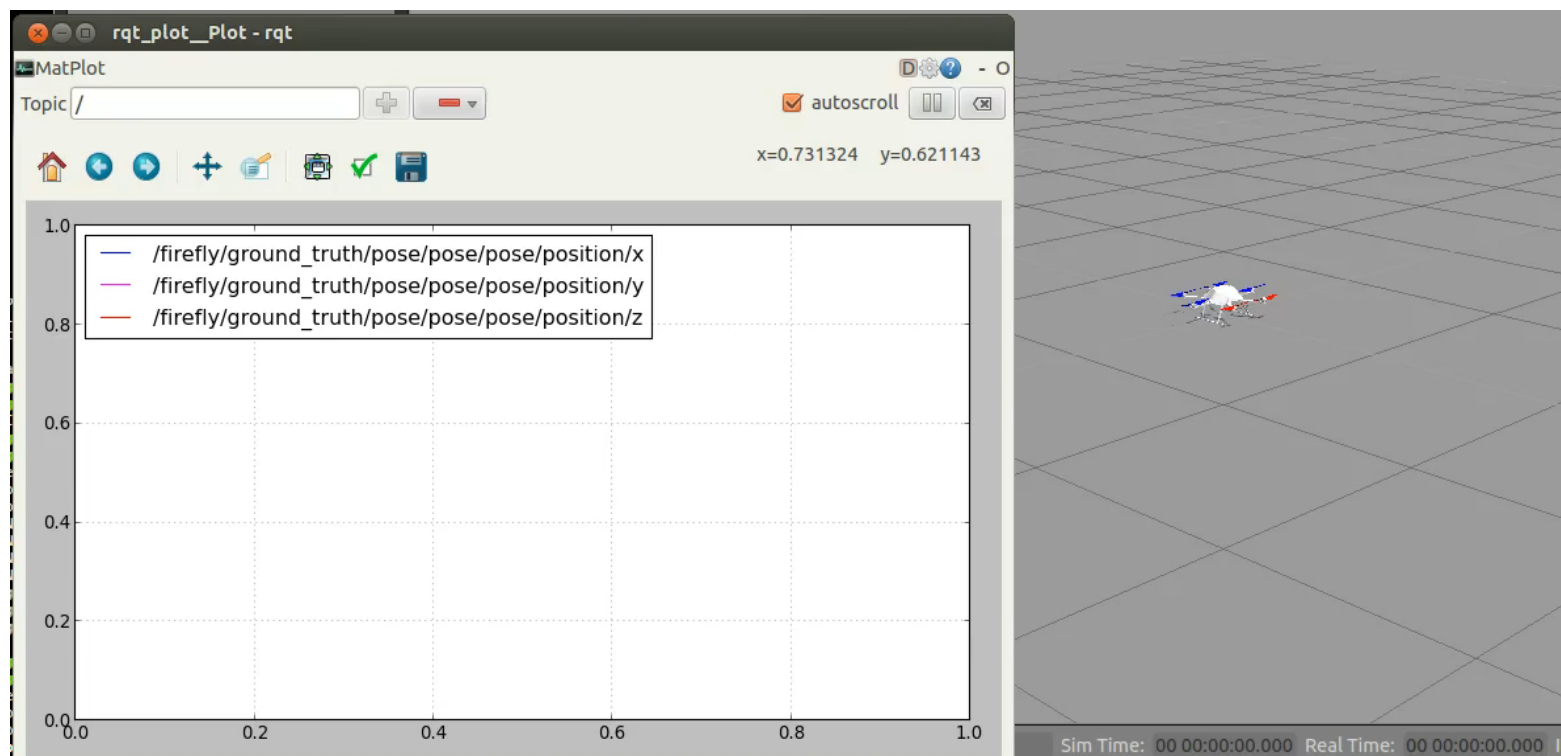
- The source code is the same for each subtask...
- ... But virtual scenarios change!
- Some common parameters need to be modified so that each subtask can be properly satisfied (mainly **control gains** and **flags**)
- These parameters may be set by defining a **launch file** for each subtask
- Solution node can then be run through the ROS command *roslaunch*

```
1 <launch>
2   <group ns="firefly">
3
4     <!-- Launch your nodes here. Extend / adapt for the subtask at hand, if necessary.-->
5
6     <node name="euroc_solution_t3" pkg="euroc_solution_t3" type="euroc_solution_t3" output="screen"/>
7     <param name="c10" value="0.5"/>
8     <param name="c12" value="0.5"/>
9     <param name="alfa" value="0.3"/>
10    <param name="beta" value="1.5"/>
11    <param name="lambda4" value="1.0"/>
12    <param name="lambda5" value="1.0"/>
13    <param name="lambda6" value="1.0"/>
14    <param name="sub_task2or3" value="1"/>
15  </group>
16 </launch>
17
```

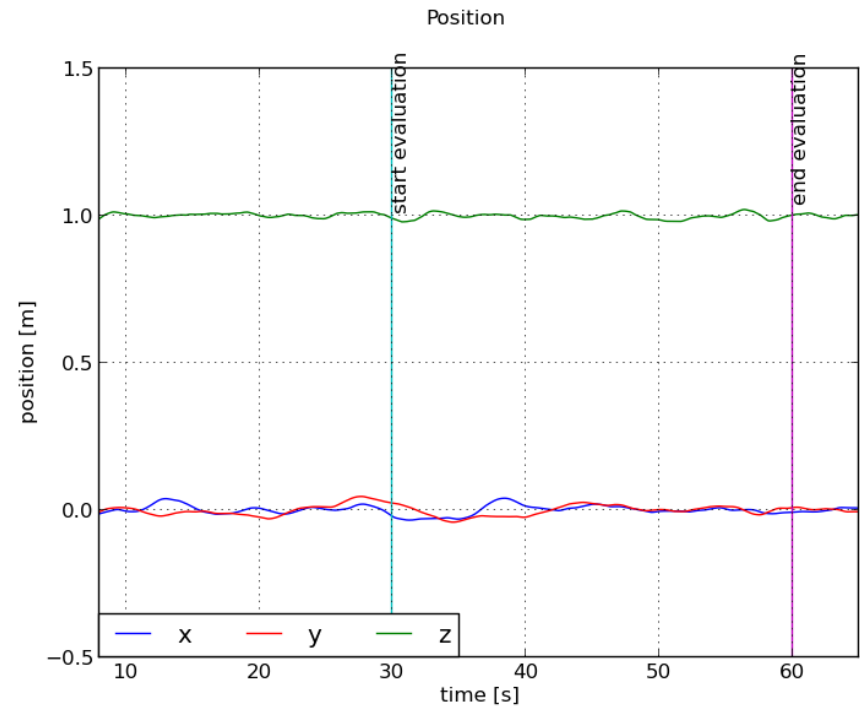
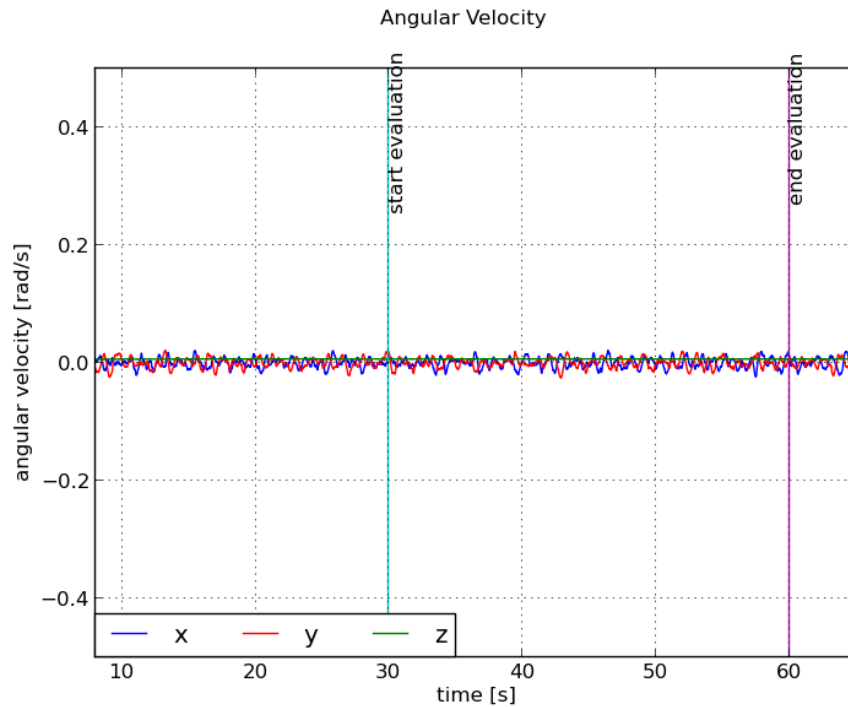
## Task 3.1: results



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## Task 3.1: results



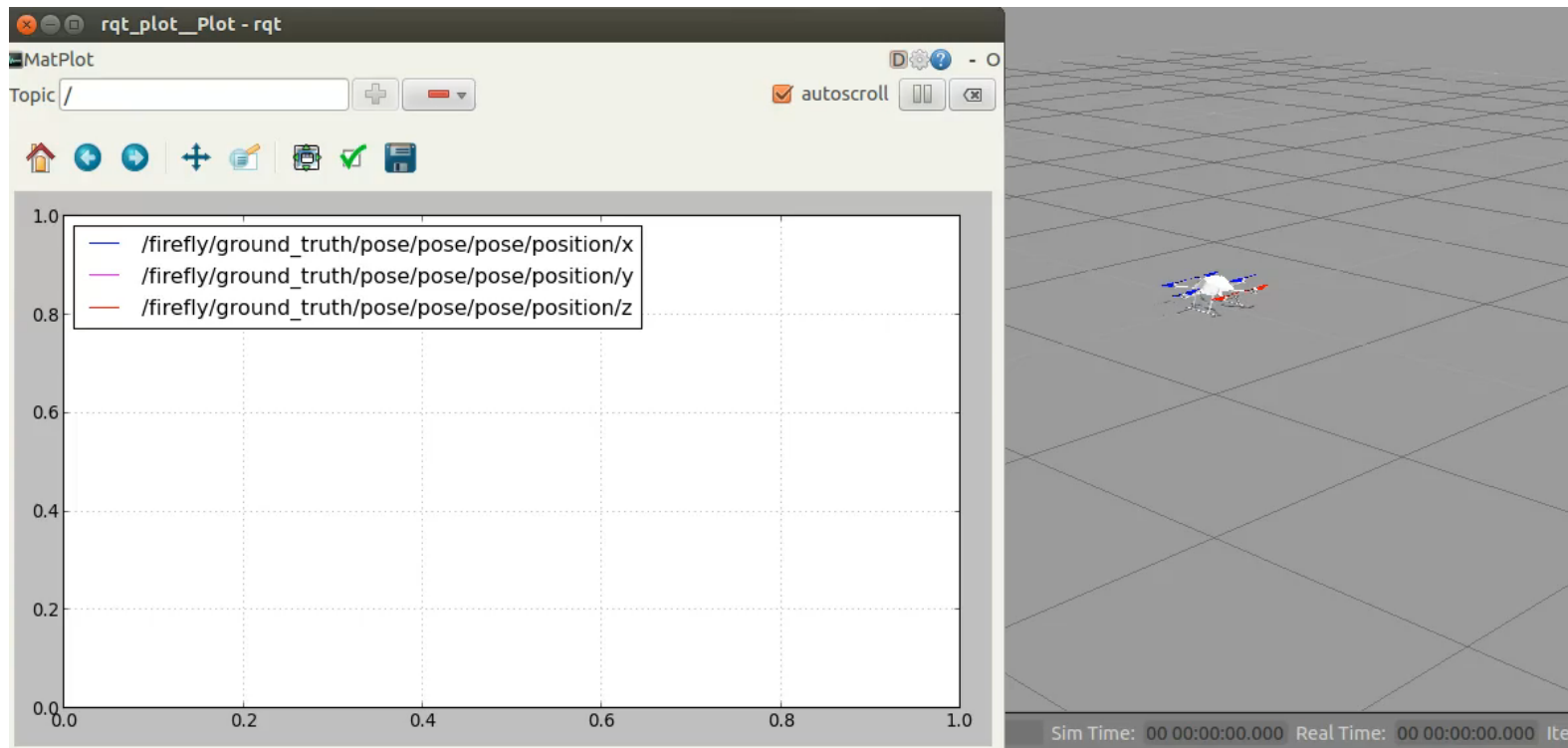
Position RMS error: 0.027 m

Angular velocity RMS error: 0.014 rad/s

Scores: 3.0, 4.5

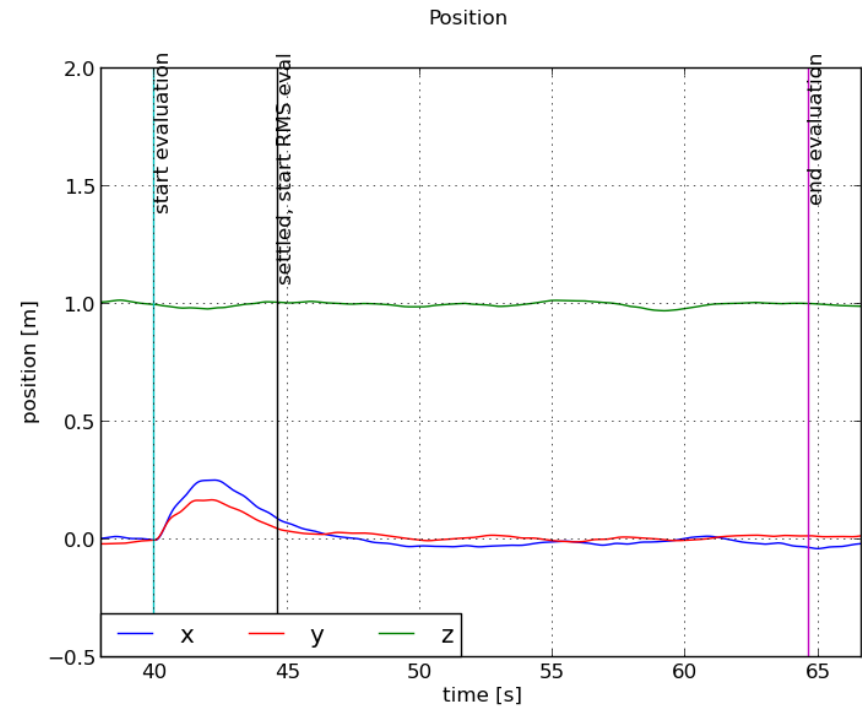
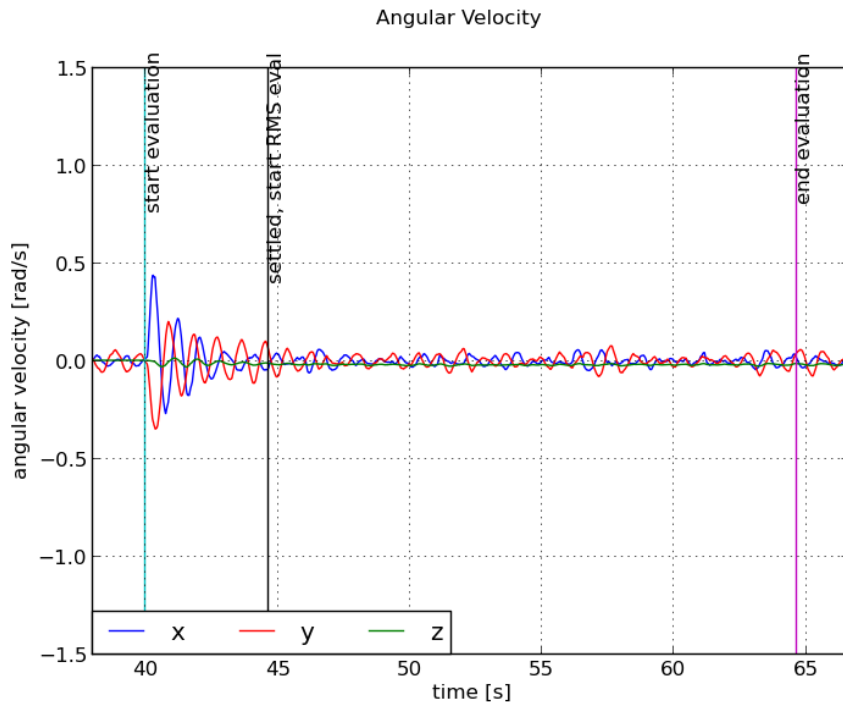
Total Score for Task 3.1 is: 7.5

## Task 3.2: results





## Task 3.2: results



Settling time: 4.630 s

Position RMS error: 0.031 m

Angular velocity RMS error: 0.041 rad/s

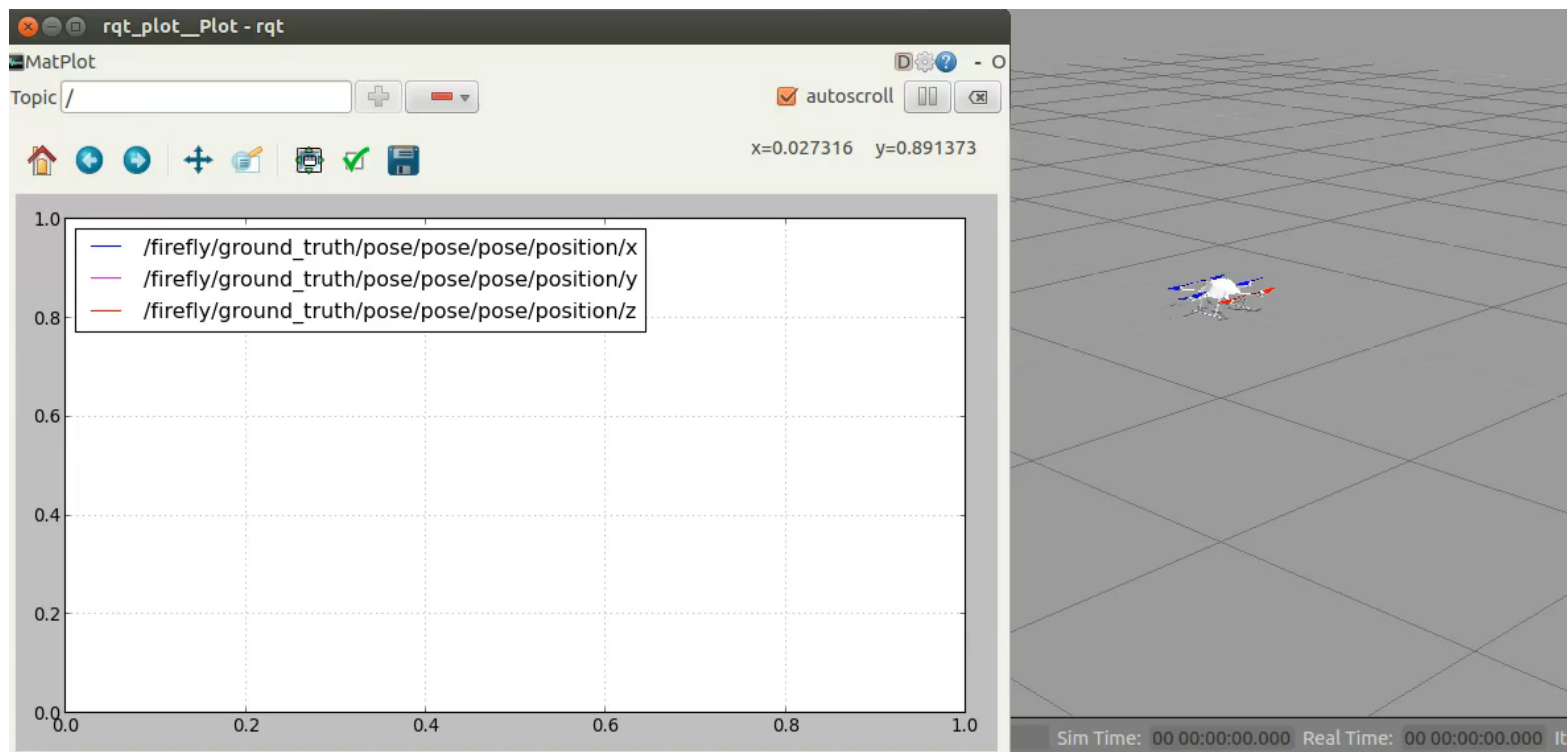
Scores: 1.0, 1.0, 1.0

Total Score for Task 3.2 is: **3.0**

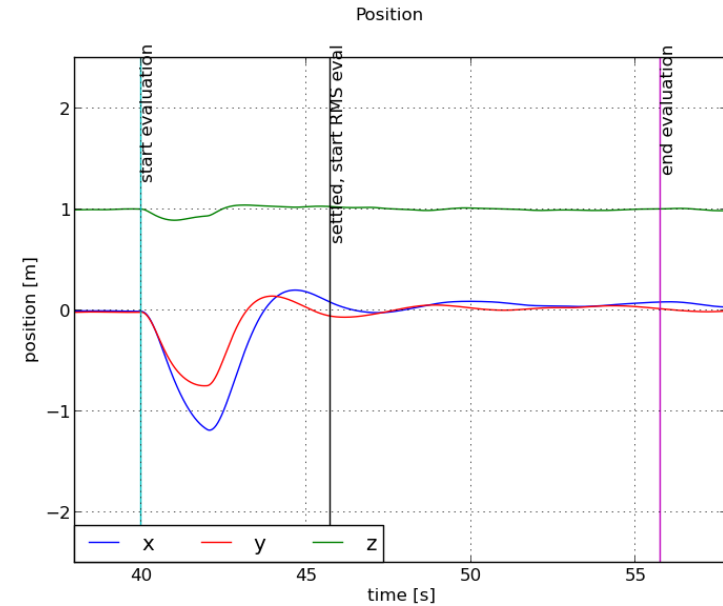
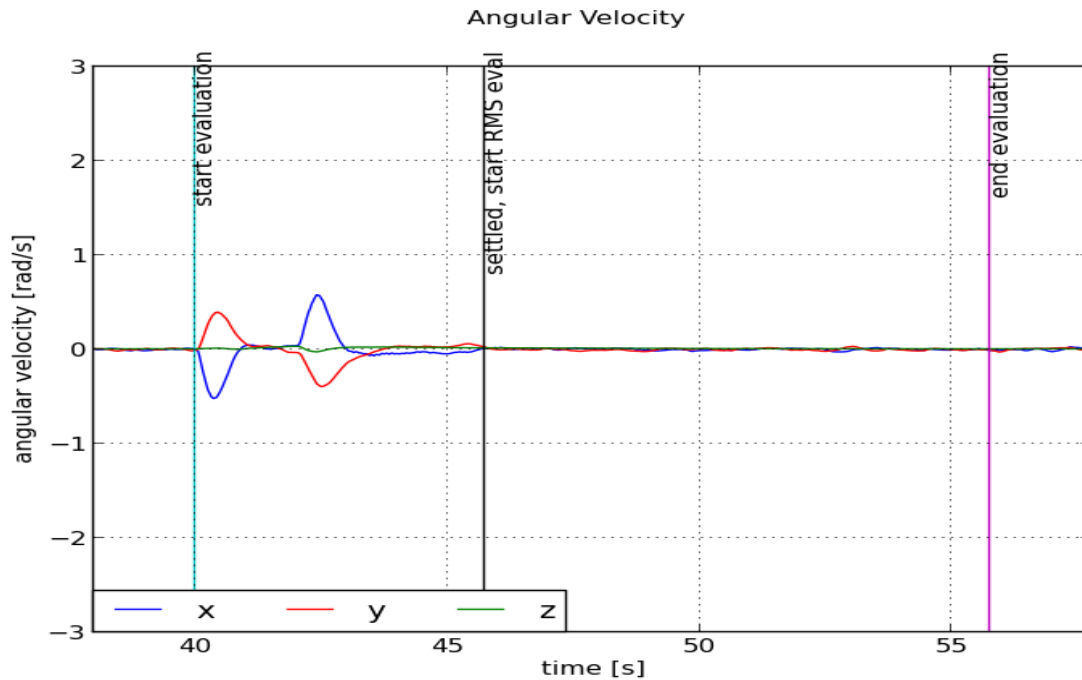
## Task 3.3: results



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## Task 3.3: results



Settling time: 5.760 s  
Position RMS error: 0.070 m  
Angular velocity RMS error: 0.017 rad/s  
Scores: 2.0, 2.0, 3.0

Total Score for Task 3.3 is: 7.0

Questions?

