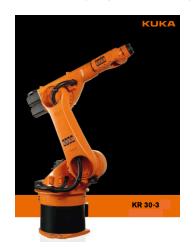
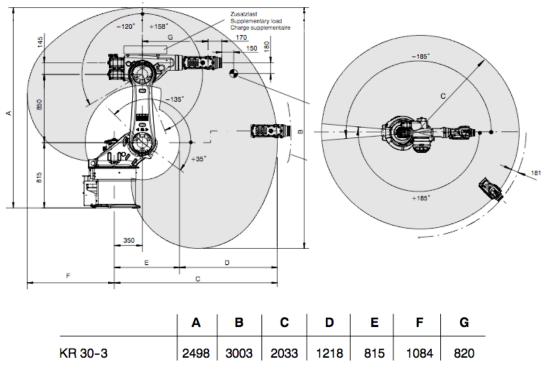
Robotics I July 7, 2010

Based on the data sheet of the KUKA KR 30-3 robot with six revolute joints and spherical wrist:

- i) assign the reference frames according to the Denavit-Hartenberg formalism, putting the origin of the reference frame RF_0 on the floor, and derive the associated table of parameters;
- *ii)* using the numerical data (in mm), determine the position of the spherical wrist center with respect to RF_0 in the configuration $\boldsymbol{\theta} = (0, \pi/2, 0, \theta_4, \theta_5, \theta_6)$, for arbitrary θ_i , i = 4, 5, 6.





[120 minutes; open books]



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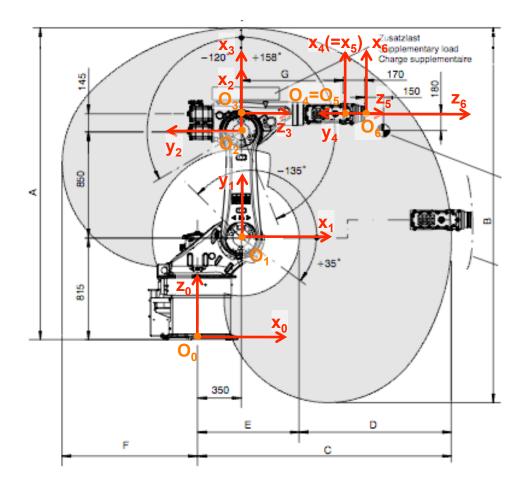


Figure 1: D-H frame assignment for the KUKA KR 30-3 robot

With reference to Fig. 1, the table of Denavit-Hartenberg parameters is the following:

i	α_i	d_i	a_i	$ heta_i$
1	$\pi/2$	$d_1 = 815$	$a_1 = 350$	θ_1
2	0	0	$a_2 = 850$	θ_2
3	$\pi/2$	0	$a_3 = 145$	θ_3
4	$-\pi/2$	$d_4 = 820$	0	θ_4
5	$\pi/2$	0	0	θ_5
6	0	$d_6 = 170$	0	θ_6

The numerical values (in mm) assigned to the constant parameters in the table are taken from the data sheet. The robot configuration shown corresponds to $\boldsymbol{\theta} = (0 \ \frac{\pi}{2} \ 0 \ 0 \ 0 \ 0)^T$. Only the first

three homogeneous transformation matrices are needed for determining the position of the center $W = 0_4 = 0_5$ of the spherical wrist:

$${}^{0}\boldsymbol{A}_{1}(\theta_{1}) = \begin{pmatrix} c_{1} & 0 & s_{1} & a_{1}c_{1} \\ s_{1} & 0 & -c_{1} & a_{1}s_{1} \\ 0 & 1 & 0 & d_{1} \\ 0 & 0 & 0 & 1 \end{pmatrix} {}^{1}\boldsymbol{A}_{2}(\theta_{2}) = \begin{pmatrix} c_{2} & -s_{2} & 0 & a_{2}c_{2} \\ s_{2} & c_{2} & 0 & a_{2}s_{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$
$${}^{2}\boldsymbol{A}_{3}(\theta_{3}) = \begin{pmatrix} c_{3} & 0 & s_{3} & a_{3}c_{3} \\ s_{3} & 0 & -c_{3} & a_{3}s_{3} \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}.$$

In fact, we may compute the position ${}^{0}\boldsymbol{p}_{04}$ of O_{4} as

$${}^{0}\boldsymbol{p}_{04,hom} = \begin{pmatrix} {}^{0}\boldsymbol{p}_{04} \\ 1 \end{pmatrix} = {}^{0}\boldsymbol{A}_{1}(\theta_{1})^{1}\boldsymbol{A}_{2}(\theta_{2})^{2}\boldsymbol{A}_{3}(\theta_{3})^{3}\boldsymbol{A}_{4}(\theta_{4}) \begin{pmatrix} \boldsymbol{0} \\ 1 \end{pmatrix}$$

but also as

$${}^{0}\boldsymbol{p}_{04,hom} = {}^{0}\boldsymbol{A}_{1}(\theta_{1}){}^{1}\boldsymbol{A}_{2}(\theta_{2}){}^{2}\boldsymbol{A}_{3}(\theta_{3}) \left(\begin{array}{c}{}^{3}\boldsymbol{p}_{34}\\1\end{array}\right) \quad \text{with} \quad {}^{3}\boldsymbol{p}_{34} = \left(\begin{array}{c}0\\0\\d_{4}\end{array}\right).$$

The most efficient way is to perform computations as matrix/vector products:

$${}^{2}\boldsymbol{p}_{24,hom} = {}^{2}\boldsymbol{A}_{3}(\theta_{3})^{3}\boldsymbol{p}_{34,hom} = \begin{pmatrix} a_{3}c_{3} + d_{4}s_{3} \\ a_{3}s_{3} - d_{4}c_{3} \\ 0 \\ 1 \end{pmatrix},$$

$${}^{1}\boldsymbol{p}_{14,hom} = {}^{1}\boldsymbol{A}_{2}(\theta_{2})^{2}\boldsymbol{p}_{24,hom} = \begin{pmatrix} (a_{2} + a_{3}c_{3} + d_{4}s_{3})c_{2} - (a_{3}s_{3} - d_{4}c_{3})s_{2} \\ (a_{2} + a_{3}c_{3} + d_{4}s_{3})s_{2} + (a_{3}s_{3} - d_{4}c_{3})c_{2} \\ 0 \\ 1 \end{pmatrix},$$

$${}^{0}\boldsymbol{p}_{04,hom} = {}^{0}\boldsymbol{A}_{1}(\theta_{1})^{1}\boldsymbol{p}_{14,hom} = \begin{pmatrix} (a_{1} + (a_{2} + a_{3}c_{3} + d_{4}s_{3})c_{2} - (a_{3}s_{3} - d_{4}c_{3})s_{2} \\ (a_{1} + (a_{2} + a_{3}c_{3} + d_{4}s_{3})c_{2} - (a_{3}s_{3} - d_{4}c_{3})s_{2})c_{1} \\ (a_{1} + (a_{2} + a_{3}c_{3} + d_{4}s_{3})c_{2} - (a_{3}s_{3} - d_{4}c_{3})s_{2})s_{1} \\ d_{1} + (a_{2} + a_{3}c_{3} + d_{4}s_{3})s_{2} + (a_{3}s_{3} - d_{4}c_{3})c_{2} \\ 1 \end{pmatrix}.$$

At the desired configuration (for the first three joints), substituting the numerical values, yields

$${}^{0}\boldsymbol{p}_{04}(0,\frac{\pi}{2},0) = \begin{pmatrix} a_1 + d_4 \\ 0 \\ d_1 + a_2 + a_3 \end{pmatrix} = \begin{pmatrix} 1170 \\ 0 \\ 1810 \end{pmatrix} \text{ [mm]}.$$

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